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PORT OF PORT LAVACA - POINT COMFORT

Providing Calhoun County Industries with Direct Deep-Draft Access to Global Markets

Bid Documents

BEAN TRACT WETLANDS CREATION PROJECT

BOARD OF COMMISSIONERS

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AUGUST 2022

SCOPE OF WORK

Scope of Work

The Calhoun Port Authority (CPA) in accordance with United States Army Corps of Engineers Permit #SWG-2016-01066, is requesting proposals for the construction of a wetland mitigation site. The proposed site is on the Bean Tract in Lavaca Bay, Calhoun County, Texas.

The proposed mitigation area is approximately 14 acres in size, with one acre of circulation channels and 3 acres of levees.

The scope of work call for the removal of material 12 acres located from CPA disposal area at the Port. This material will be transported to the proposed site. At the site an access road will be constructed to facilitate the movement of material. Two temporary access roads will be constructed from the shoreline to the proposed mitigation area. The roads 70-ft in surface width, roads have been designed to avoid impacts to wetlands and other sensitive resources. These roads are to be removed upon completion of the construction and pre-construction contours restored.

Protection levees will be constructed with a minimum base of 45 feet wide and built up to an elevation of +10 ft NAVD 88 to accommodate equipment movement and material placement. Approximately 1,775 linear ft of articulated mat is to be installed to provide stabilization of the levee from wind and wave energy. The finished grade of the armored levee would be +5.0 ft NAVD 88. The finished grade of unarmored levee will be between +2.0 ft and +3.0 ft NAVD 88 to allow for tidal influence. Circulation channels will be lowered to -2.0 to -3.0 ft NAVD 88 with a 20-ft top width. All slopes to be a minimum of 3:1.

SCOPE OF WORK:

PROPOSED LEVEE - BEAN TRACT MITIGATION SITE SEPTEMBER 2022, LLOYD ENGINEERING



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POINT COMFORT, TEXAS

CALHOUN PORT AUTHORITY

PROPOSED LEVEE - BEAN TRACT MITIGATION SITE

ISSUED FOR BIDDING

SEPTEMBER 2022





DRAWING INDEX SHEET NUMBER SHEET TITLE

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C1.1	PROPOSED ROADWAY SITE PLAN
C1.2	TYPICAL ROAD DETAILS
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C3.3	BORROW AREA SITE PLAN

GENERAL:

- 1. ALL ELEVATIONS SHOWN REFERENCE NAVD 88.
- 2. CONTRACTOR SHALL FIELD CHECK AND VERIFY ALL ELEVATIONS, COORDINATES, DIMENSIONS, EXISTING CONDITIONS, AND INFORMATION INDICATED ON THE CONTRACT DOCUMENTS PRIOR TO COMMENCEMENT OF SITE WORK. THE OWNER SHALL BE NOTIFIED IMMEDIATELY OF ANY DISCREPANCIES FOUND ON THE CONTRACT DOCUMENTS OR FOUND TO EXIST BETWEEN THE FIELD CONDITIONS AND THE CONTRACT DOCUMENTS. THE CONTRACTOR SHALL TAKE CORRECTIVE ACTION AS DIRECTED BY THE OWNER.
- 3. CONTRACTOR SHALL SUBMIT STORM WATER POLLUTION PREVENTION PLAN (SW3P) TO THE OWNER. CONSTRUCTION ACTIVITY MAY NOT COMMENCE UNIT SW3P IS APPROVED BY THE OWNER
- 4. THE TEXAS ONE CALL SYSTEM SHALL BE NOTIFIED 48-HOURS PRIOR TO EXCAVATING. THIS ACTION HOWEVER, SHALL IN NO WAY BE INTERPRETED AS RELIEVING THE CONTRACTOR OF THE RESPONSIBILITY UNDER THE TERMS OF THE CONTRACT AS SET OUT IN THE PLANS AND SPECIFICATIONS. THE CONTRACTOR SHALL REPAIR ANY DAMAGE CAUSED BY HIS OPERATIONS AT HIS OWN EXPENSE AND TO THE SATISFACTION OF THE UTILITY COMPANY INVOLVED.
- 5. THE CONTRACTOR SHALL COMPLY WITH ALL PROVISIONS OF THE US ARMY CORPS OF ENGINEERS (USACE) PERMIT OBTAINED BY THE OWNER FOR THIS PROJECT. REFER TO US ARMY CORPS OF ENGINEERS PERMIT NO. SWG-2016-01066.
- 6. CONTRACTOR SHALL CONDUCT HIS OPERATIONS SO AS TO NOT INTERFERE WITH, OR BE DETRIMENTAL TO VESSEL AND VEHICULAR TRAFFIC AND THE DAILY OPERATION OF THE OWNER DURING THE COURSE OF THE WORK
- 7. THE LOCATION AND DEPTH OF UTILITIES AND PIPELINES SHOWN ARE APPROXIMATE AND SHALL BE VERIFIED BY THE CONTRACTOR BEFORE WORK COMMENCES. PRIOR TO BEGINNING ANY EXCAVATION WORK IN THE AREA OF EXISTING UTILITIES OR PIPELINES, THE CONTRACTOR SHALL CONTACT THE UTILITY OR PIPELINE COMPANIES OWNER FOR EXACT LOCATIONS AND DEPTHS TO PREVENT ANY DAMAGE OR INTERFERENCE WITH PRESENT FACILITIES
- 8. THE TEXAS ONE CALL SYSTEM SHALL BE NOTIFIED 48-HOURS PRIOR TO EXCAVATING. THIS ACTION HOWEVER, SHALL IN NO WAY BE INTERPRETED AS RELIEVING THE CONTRACTOR OF THE RESPONSIBILITY UNDER THE TERMS OF THE CONTRACT AS SET OUT IN THE PLANS AND SPECIFICATIONS. THE CONTRACTOR SHALL REPAIR ANY DAMAGE CAUSED BY HIS OPERATIONS AT HIS OWN EXPENSE AND TO THE SATISFACTION OF THE UTILITY OR PIPELINE COMPANY INVOLVED.
- 9. ALL EXISTING ROADWAYS AND OTHER FEATURES WHICH ARE DAMAGED BY THE CONTRACTOR SHALL BE REPAIRED AT THE CONTRACTOR'S EXPENSE TO THE SATISFACTION OF THE OWNER.
- WORKER SAFETY IN EXCAVATIONS AND TRENCHES SHALL BE PROVIDED BY THE CONTRACTOR IN ACCORDANCE WITH OCCUPATIONAL SAFETY AND HEALTH ADMINISTRATION (OSHA) STANDARDS, 29 CFR 1926, SUBPART P - EXCAVATIONS, TRENCHING, AND SHORING, COMPLY WITH USACE-EM-385 FOR ALL ASPECTS OF CONSTRUCTION.

HORIZONTAL AND VERTICAL CONTROL:

- 1. TOPOGRAPHIC SURVEY WAS PERFORMED BY CRA ASSOCIATES, DATED NOVEMBER 2019.
- 2. HYDROGRAPHIC SURVEY WAS PERFORMED BY CRA ASSOCIATES, DATED NOVEMBER 2019.
- 3. COORDINATES SHOWN ARE STATE PLANE GRID, TEXAS SOUTH CENTRAL ZONE, IN U.S. FEET.
- 4. ALL ELEVATIONS SHOWN REFER TO US CORPS OF ENGINEERS MEAN LOWER LOW WATER (MLLW) DATUM

LEVEE/TEMPORARY BERM CONSTRUCTION:

- SEMI-COMPACTED FILL SHALL BE PLACED WITH SUITABLE EQUIPMENT IN UNIFORM LAYERS WHICH, BEFORE COMPACTION, SHALL NOT EXCEED 12 TO 24 INCHES IN THICKNESS. EACH LAYER SHALL BE COMPACTED BY NOT LESS THAN THREE (3) COVERAGE OF A CRAWLER-TYPE TRACTOR D-5.
- 2. GEOTEXTILE FABRIC TO BE MIRAFI 500X OR EQUAL.
- .3 ARTICULATED CONCRETE MATTRESS TO BE ARMORELEX CLASS 70 MAT OR FOUND
- 4. CONTRACTOR SHALL ANTICIPATE SATURATED GROUND CONDITIONS AT THE SITE AND APPLY APPROPRIATE MEANS AND METHODS FOR CONSTRUCTING IN SOFT WET SOILS.
- 5. USE RIPRAP PER TXDOT ITEM 432. SEE GRADATION BELOW:

RIPRAP GRADATION NO. 1								
	STONE LB	WEIGHT S.	VOLUME FT (CUBIC (2)	CUBICAL SHAPE FT (EACH SIDE)		SPHERICAL SHAPE FT (DIA.)	
PERCENT LIGHTER BY WEIGHT	LOWER LIMIT	UPPER LIMIT	LOWER LIMIT	UPPER LIMIT	LOWER LIMIT	UPPER LIMIT	LOWER LIMIT	UPPER LIMIT
100	180	265	1.20	1.77	1.06	1.21	1.31	1.50
50	80	110	0.53	0.73	0.81	0.90	1.01	1.12
15	40	60	0.27	0.40	0.64	0.74	0.80	0.91

EMBANKMENT:

1. MATERIALS THAT ARE CLASSIFIED IN ACCORDANCE WITH ASTM D 2487 AS CL WITH LESS THAN 35 PERCENT SAND CONTENT ARE SUITABLE FOR USE AS EMBANKMENT FILL. MATERIALS CLASSIFIED AS CL-ML OR ML ARE NOT SUITABLE. SEE TABLE 1. ALL FILL MATERIALS SHALL BE FREE FROM MASSES OF ORGANIC MATTER, STICKS, BRANCHES, ROOTS, AND OTHER DEBRIS, INCLUDING HAZARDOUS AND REGULATED SOLID WASTES. LARGE CLAY CLODS SHALL BE PULVERIZED AND REDUCED TO LESS THAN 1/2 INCH IN DIAMETER. AS EARTH FROM THE DESIGNATED EXCAVATION AREAS MAY CONTAIN EXCESSIVE AMOUNTS OF WOOD, ISOLATED PIECES OF WOOD WILL NOT BE CONSIDERED OBJECTIONABLE IN THE EMBANKMENT PROVIDED THEIR SIZE DOES NOT EXCEED ONE INCH IN DIAMETER. NOT MORE THAN 1 PERCENT (BY VOLUME) OF OBJECTIONABLE MATERIAL SHALL BE CONTAINED IN THE EARTH MATERIAL PLACED IN EACH CUBIC YARD OF THE LEVEE SECTION. POCKETS AND/OR ZONES OF WOOD SHALL NOT BE PLACED IN THE EMBANKMENT.

2. MATERIALS PLACED IN THE SECTION MUST HAVE A MINIMUM OF 60% PASSING THE NO. 200 SIEVE AS DETERMINED BY ASTM D422. ALSO, MATERIALS PLACED IN THIS SECTION SHALL BE AT OR BELOW ORGANIC CONTENT OF 9 PERCENT BY WEIGHT AS DETERMINED BY ASTM D 2974, METHOD C. MATERIALS PLACED IN THE SECTION MUST CONTAIN LESS THAN 35 PERCENT SAND CONTENT BY WEIGHT AS DETERMINED BY ASTM D 1140.

FILL MATERIAL:

1. DO NOT CONDUCT PLACEMENT OPERATIONS DURING INCLEMENT WEATHER OR WHEN EXISTING GROUND OR FILL MATERIALS EXCEED 3 PERCENT OF OPTIMUM MOISTURE CONTENT. CONTRACTOR MAY MANIPULATE WET MATERIAL TO FACILITATE DRYING. BY DISKING OR WIND ROWING, EACH LAYER SHALL BE HOMOGENEOUS AND CONTAIN UNIFORM MOISTURE CONTENT BEFORE COMPACTION. MIX DISSIMILAR ABUTTING MATERIALS TO PREVENT ABRUPT CHANGES IN COMPOSITION OF FILL. LAYERS SHALL NOT EXCEED 12 INCHES OF COMPACTED THICKNESS.

COMPACT TO MINIMUM DENSITY OF 90 PERCENT OF MAXIMUM DRY DENSITY AT MOISTURE CONTENT OF OPTIMUM TO 3 PERCENT ABOVE OPTIMUM AS DETERMINED BY ASTM D 698.

- 2. UNSUITABLE MATERIAL: UNSUITABLE SOIL MATERIALS ARE THE FOLLOWING:
- MATERIALS CLASSIFIED AS ML, CL-ML, MH, PT, OH, AND OL ACCORDING TO ASTM D 2487.
- MATERIALS THAT CANNOT BE COMPACTED TO REQUIRED DENSITY DUE TO GRADATION, PLASTICITY, OR MOISTURE CONTENT.
- MATERIALS THAT CONTAIN LARGE CLODS, AGGREGATES, STONES GREATER THAN 4 INCHES IN
- ANY DIMENSION, DEBRIS, VEGETATION, WASTE OR ANY OTHER DELETERIOUS MATERIALS. • MATERIALS THAT ARE CONTAMINATED WITH HYDROCARBONS OR OTHER CHEMICAL
- CONTAMINANTS.

3. SUITABLE MATERIAL: INORGANIC FAT CLAYS (CH) MAY BE USED AS INORGANIC EMBANKMENT MATERIAL. WHEN REQUIRED DENSITY IS NOT ACHIEVED, REWORK, DRY OUT, USE LIME STABILIZATION OR OTHER APPROVED METHODS TO ACHIEVE COMPACTION REQUIREMENTS, OR USE DIFFERENT SUITABLE MATERIAL. MAXIMUM 9-INCH COMPACTED LIFT THICKNESS FOR CLAYEY SOILS AND MAXIMUM 12-INCH LIFT THICKNESS FOR GRANULAR SOILS. COMPACT TO MINIMUM OF 90 PERCENT OF MAXIMUM DRY DENSITY DETERMINED ACCORDING TO ASTM 698. THE LIQUID LIMIT SHALL BE 50 OR GREATER. GRADATION SHALL INCLUDE 50% OR GREATER PASSING SLEEVE 200.

CEMENT STABILIZED SAND:

- 1. PLACE SAND-CEMENT MIXTURE IN MAXIMUM 12-INCH-THICK LOOSE LIFTS AND COMPACT TO 95% OF MAXIMUM DRY DENSITY AS DETERMINED IN ACCORDANCE WITH ASTM D558. TARGET MOISTURE CONTENT DURING COMPACTION IS ±3% OF OPTIMUM.
- 2. DO NOT PLACE OR COMPACT SAND-CEMENT MIXTURE IN STANDING OR FREE WATER.
- 3. USE SAND-CEMENT MIXTURE PRODUCING MINIMUM UNCONFINED COMPRESSIVE STRENGTH OF 150 POUND PER SQUARE INCH IN 48 HOURS
- 4. PROVIDE 1.5 SACK OF CEMENT PER TON OF DRY SAND. CEMENT SHALL BE TYPE 1 PORTLAND CEMENT CONFORMING TO ASTM C150.
- 5. SAND SHALL BE CLEAN AND FREE OF ORGANICS WITH A PLASTICITY INDEX OF 4 OR LESS WHEN TESTED IN ACCORDANCE WITH ASTM D4318.

ROADWAY PREPARATION:

- 1. FOLLOWING GRUBBING AND REMOVAL OF DELETERIOUS MATTER FROM THE EXISTING SURFACE AND AFTER CUT GRADES HAVE BEEN ESTABLISHED, THE EXPOSED SOIL SHOULD BE EXCAVATED TO AT LEAST TWO FEET BELOW DESIGN TOP-OF-SUBGRADE ELEVATION OR EXISTING GRADE, WHICHEVER IS DEEPER. THE OVER-EXCAVATION SHOULD EXTEND AT LEAST 3, AND PREFERABLY 5, FEET BEYOND THE LIMITS OF THE AREA TO RECEIVE SURFACE TREATMENT. IF POOR OR DELETERIOUS MATERIAL IS ENCOUNTERED AT THE BASE OF THE 2-FOOT OVER-EXCAVATION, ADDITIONAL OVER-EXCAVATION MAY BE REQUIRED AS RECOMMENDED BY THE GEOTECHNICAL ENGINEER. THE OVER-EXCAVATION MAY BE TERMINATED IF COMPETENT NATURAL SOILS (I.E., MEDIUM DENSE SANDS OR STIFF COHESIVE SOILS) ARE ENCOUNTERED.
- 2. OVER-EXCAVATED AREAS SHOULD BE BACKFILLED WITH PROPERLY PLACED AND COMPACTED STRUCTURAL (SELECT) FILL TO ATTAIN DESIGN TOP-OF-SUBGRADE ELEVATION. STRUCTURAL FUL MAY CONSIST OF LOW PLASTICITY COHESIVE SOUS OR SANDY SOUS COHESIVE SOUS SHOULD HAVE A LIQUID LIMIT OF LESS THAN 40, A PLASTICITY INDEX BETWEEN 12 AND 30, AND A FINES CONTENT (I.E., PASSING THE NO. 200 SIEVE) BETWEEN 60 AND 85 PERCENT. STRUCTURAL FILL SHOULD BE FREE OF DELETERIOUS MATTER AND SHOULD HAVE AN EFFECTIVE CLOD DIAMETER LESS THAN 3 INCHES. STRUCTURAL FILL SHOULD BE PLACED IN MAXIMUM 8-INCH-THICK LOOSE LIFTS AND UNIFORMLY COMPACTED TO AT LEAST 95 PERCENT OF THE MAXIMUM DRY DENSITY. COHESIVE SOILS SHOULD BE PLACED AT A MOISTURE CONTENT OF 1 PERCENT "DRY" TO 3 PERCENT "WET" OF OPTIMUM AS DETERMINED BY ASTM D698 (STANDARD PROCTOR); THE MOISTURE CONTENT OF SANDY SOILS MAY BE WITHIN 3 PERCENT OF OPTIMUM. OVEREXCÂVATED ONSITE SOILS MEETING THE REQUIREMENTS OF STRUCTURAL FILL MAY BE RF-USED
- 3. THE SUBGRADE PREPARATION SHOULD EXTEND LATERALLY AT LEAST 3, AND PREFERABLY 5, FEET BEYOND THE EDGES OF THE AREAS TO RECEIVE SURFACE COVER. PRIOR TO PLACEMENT OF STRUCTURAL FILL TO BRING OVER-EXCAVATED AREAS TO DESIGN TOP-OF-SUBGRADE, THE EXPOSED SOILS SHOULD BE PROOFROLLED TO IDENTIFY AREAS OF UNSUITABLE SOILS AS DISCUSSED BELOW.

PROOF-ROLLING:

- 1. FOR LARGE AND EXPOSED AREAS, PROOF-ROLLING OF THE SUBGRADE SHOULD BE PERFORMED. WE RECOMMEND THAT PROOF-ROLLING BE PERFORMED USING A FULLY-LOADED DUMP TRUCK OR WATER TRUCK WITH A WEIGHT OF AT LEAST 20 TONS AND A TIRE PRESSURE OF AT LEAST 70 PSI. DO NOT RECOMMEND USE OF OFF-ROAD EARTH MOVING EQUIPMENT, COMPACTORS, OR TRACK-MOUNTED VEHICLES FOR PROOF-ROLLING. PROOF-ROLLING SHOULD EXTEND AT LEAST 3 FEET AND PREFERABLY 5 FEET (RIGHT-OF-WAY PERMITTING) BEYOND THE FOOTPRINT OF THE STUDY SITE
- 2. PROOF-ROLLING SPECIFICATIONS SHOULD PROVIDE FOR RUT DEPTHS LESS THAN 1 INCH AND NO VISUAL EVIDENCE OF PUMPING. AREAS OF SUBGRADE SOILS WHERE RUTTING IN EXCESS OF 1 INCH OR PUMPING ARE OBSERVED SHOULD BE REMOVED TO EXPOSE COMPETENT SOILS AND REPLACED WITH PROPERLY COMPACTED STRUCTURAL FILL

SUBGRADE TREATMENT:

AGGREGATE-SURFACED AREA:

GUIDE MANUAL (AUGUST 2015).

Recommended Grada

Figure	Base Aggregate Layer	Surface Aggregate Layer		
Sieve	Percent Passing	Percent Passing		
1″	100			
3/4"	80 - 100	100		
1/2″	68-91			
No. 4	46 - 70	50 - 78		
No. 8	34 - 54	37 - 67		
No. 40	13 - 35	13 - 35		
No. 200	3 - 12	4 - 15**		
Plasticity Index	0-6	4 - 12		

LIME:

- ABOUT 6-8% LIME, BY DRY WEIGHT MAY BE REQUIRED.
- LISTED IN CHEMICAL COMPOSITION CHART.
- PURPOSE INTENDED
- PLACING.
- 5 CONFORM TO THE FOLLOWING REQUIREMENTS.

	TYPE							
CHEMICAL COMPOSITION	A	В	С					
Active lime content, % by weight Ca(OH) ₂ +CaO	90.0 min ¹	87.0 min ²	-					
Unhydrated lime content, % by weight CaO	5.0 max	-	87.0 min					
Free water content, % by weight H2O :	5.0 max	-	-					
SIZING								
Wet Sieve, as % by weight residue retained:								
No. 6	0.2 max	0.2 max ²	8.0 max ³					
No. 30	4.0 max	4.0 max ²	-					
Dry sieve, as % by weight residue retained:								
1-inch	-	-	0.0					
1/2-inch	-	-	10.0 max					
 Notes: Maximum 5.0% by weight CaO shall be all content. Maximum solids content of slurry. Total active lime content, as CaO, in materi 2.0% by weight of original Type C lime 	 Notes: Maximum 5.0% by weight CaO shall be allowed in determining total active lime content. Maximum solids content of slurry. Total active lime content, as CaO, in material retained on No. 6 sieve shall not exceed 2.0% by weight of original Type C lime. 							
6. LIME CONTAINING MAGNESIUM HYDROX	IDE IS PRO	HIBITED.						

3. SCHEDULE PROOF-ROLLING ACTIVITIES DURING A RELATIVELY DRY PERIOD. DO NOT ALLOW PROOF-ROLLING ACTIVITIES TO BEGIN DURING OR IMMEDIATELY AFTER A SIGNIFICANT RAIN EVENT. THE GEOTECHNICAL ENGINEER-OF-RECORD (GER) SHOULD BE CONTACTED TO EVALUATE THE SITE CONDITIONS IF A LARGE RAINFALL EVENT OCCURS DURING SUBGRADE PREPARATION.

1. FOR SUBGRADE IMPROVEMENT, COHESIVE SOILS AND STRUCTURAL FILL SHOULD BE TREATED WITH LIME, WHILE COHESIONLESS (SANDY TO SILTY SOILS) SHOULD BE TREATED WITH LIME.

1. THE AGGREGATE-SURFACED PARKING/STORAGE/LAYOUT AREA SHOULD BE DESIGNED IN ACCORDANCE WITH AASHTO GUIDE FOR DESIGN OF PAVEMENT STRUCTURE (1993 EDITION). AND FEDERAL HIGHWAY ADMINISTRATION (FHWA) GRAVEL ROADS CONSTRUCTION AND MAINTENANCE

tions	for	Base a	nd	Surface	Aggregate	Layers
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1. THE OPTIMUM LIME CONTENT IS THE AMOUNT OF LIME NECESSARY TO ACHIEVE A PH OF 12.0. WHILE TRYING TO ACHIEVE PLASTICITY (PI) OF LESS THAN 2.0. FOR ESTIMATION PURPOSES,

2. TYPE A - HYDRATED LIME: DRY MATERIAL CONSISTING ESSENTIALLY OF CALCIUM HYDROXIDE OR MIXTURE OF CALCIUM HYDROXIDE AND AN ALLOWABLE PERCENTAGE OF CALCIUM OXIDE AS

3. TYPE B - COMMERCIAL LIME SLURRY: LIQUID MIXTURE CONSISTING ESSENTIALLY OF LIME SOLIDS AND WATER IN SLURRY FORM. WATER OR LIQUID PORTION SHALL NOT CONTAIN DISSOLVED MATERIAL IN SUFFICIENT QUANTITY TO BE INJURIOUS OR OBJECTIONABLE FOR

4. TYPE C - QUICKLIME: DRY MATERIAL CONSISTING ESSENTIALLY OF CALCIUM OXIDE: MATERIALS SHALL BE: FINELY-GRADED QUICKLIME FOR USE IN PREPARATION OF SLURRY FOR WET

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	Texas Registered Engineering Firm F-02846	Construction Management Design Dredge Inspections Owner's Engineer Permitting Assistance	6565 West Loop South Houston, Texas 77401 (832)426-4656
	CALHOUN PORT AUTHORITY BEAN TRACT WETLAND	GENERAL NOTES	1 OF 2
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LIME SLURRY APPLICATION:

- 1. MINIMUM LIME CONTENT SHALL BE 5 PERCENT OF DRY UNIT WEIGHT OF SUBGRADE AS DETERMINED BY ASTM D 698.
- 2. CURE SOIL LIME MATERIAL FOR 24 TO 72 HOURS OR AS REQUIRED TO OBTAIN OPTIMUM HYDRATION. KEEP SUBGRADE MOIST DURING CURE.
- 3. MIX AND PULVERIZE UNTIL ALL MATERIAL PASSES 13/4-INCH SIEVE; MINIMUM OF 85 PERCENT, EXCLUDING NON-SLACKING FRACTIONS, PASSES 3/4-INCH SIEVE; AND MINIMUM OF 60 PERCENT EXCLUDING NON-SLACKING FRACTIONS PASSES NO. 4 SIEVE. TEST ACCORDING TO TXDOT TEX-101-E, PART III USING DRY METHOD.
- 4. DO NOT EXPOSE HYDRATED LIME TO OPEN AIR FOR 6 HOURS OR MORE DURING INTERVAL BETWEEN APPLICATION AND MIXING. AVOID EXCESSIVE HYDRATED LIME LOSS DUE TO WASHING OR BLOWING.

COMPACTION:

- 1. AERATE OR SPRINKLE TO ATTAIN OPTIMUM MOISTURE CONTENT TO 3 PERCENT ABOVE OPTIMUM, AS DETERMINED BY ASTM D 698 ON MATERIAL SAMPLE FROM ROADWAY AFTER FINAL MIX WITH LIME.
- 2. START COMPACTION IMMEDIATELY AFTER FINAL MIXING.
- 3. DO NOT ALLOW STABILIZED SUBGRADE TO MIX WITH UNDERLYING MATERIAL. CORRECT IRREGULARITIES OR WEAK SPOTS IMMEDIATELY BY REPLACING MATERIAL AND RECOMPACTING.
- 4. COMPACT SUBGRADE TO MINIMUM DENSITY OF 95 PERCENT OF MAXIMUM DRY DENSITY, ACCORDING TO ASTM D 698, AT MOISTURE CONTENT OF OPTIMUM TO 3 PERCENT ABOVE OPTIMUM, UNLESS OTHERWISE INDICATED ON DRAWINGS.
- 5. SEAL WITH APPROVED LIGHT PNEUMATIC TIRED ROLLERS. PREVENT SURFACE HAIR LINE CRACKING. REWORK AND RECOMPACT AT AREAS WHERE HAIRLINE CRACKING DEVELOP.

CURING:

- 1. MOIST CURE FOR MINIMUM OF 3 DAYS BEFORE PLACING BASE OR SURFACE COURSE, OR OPENING TO TRAFFIC. SUBGRADE MAY BE OPENED TO TRAFFIC AFTER 2 DAYS WHEN ADEQUATE STRENGTH HAS BEEN ATTAINED TO PREVENT DAMAGE. RESTRICT TRAFFIC TO LIGHT PNEUMATIC ROLLERS OR VEHICLES WEIGHING LESS THAN 10 TONS.
- 2. PLACE BASE OR SURFACE WITHIN 14 DAYS AFTER FINAL MIXING AND COMPACTION. RESTART COMPACTION AND MOISTURE CONTENT OF BASE MATERIAL WHEN TIME IS EXCEEDED.

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Texas Registered Engineering Firm F-02846 ENGINEERING, INC.	Construction Management Design Dredge Inspections Owner's Engineer Permitting Assistance 6565 West Loop South Houston, Texas 77401 (832)426-4856
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* CONVENTIONAL ROADS ONLY

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SCOPE OF WORK:

GEOTECHNICAL SUBSURFACE INVESTIGATION AND RECOMMENDATIONS FOR THE PROPOSED BENEFICIAL USE MITIGATION



- GEOTECHNICAL ENGINEERING
- MATERIALS ENGINEERING & TESTING
- SOILS ASPHALT CONCRETE

GEOTECHNICAL SUBSURFACE INVESTIGATION AND RECOMMENDATIONS FOR THE PROPOSED BENEFICIAL USE MITIGATION; PORT OF PORT LAVACA (SWG-2016-01066) CALHOUN COUNTY, TEXAS

RETL REPORT NUMBER: G122209

PREPARED FOR:

BELAIRE ENVIRONMENTAL, INC. P.O. BOX 741 ROCKPORT, TEXAS 78381

MAY 31, 2022

PREPARED BY:

ROCK ENGINEERING & TESTING LABORATORY, INC. 6817 LEOPARD STREET CORPUS CHRISTI, TEXAS 78409 P: (361) 883-4555; F: (361) 883-4711 TBPE FIRM NO. 2101



GEOTECHNICAL ENGINEERING

- CONSTRUCTION MATERIALS
 ENGINEERING & TESTING
- SOILS ASPHALT CONCRETE

May 31, 2022

Belaire Environmental, Inc. P.O. Box 741 Rockport, Texas 78381

Attention: Ms. Laura Fox

SUBJECT: SUBSURFACE INVESTIGATION, LABORATOY TESTING PROGRAM, AND GEOTECHNICAL RECOMMENDATIONS FOR THE PROPOSED BENEFICIAL USE MITIGATION; PORT OF PORT LAVACA (SWG-2016-01066) Calhoun County, Texas RETL Job No. – G122209

Dear Ms. Fox,

In accordance with our agreement, we have conducted a subsurface investigation, laboratory testing program, and geotechnical evaluation for the above referenced project. The results of this investigation, together with our recommendations, are to be found in the accompanying report, one electronic copy of which is being transmitted herewith for your records and distribution to the design team.

Often, because of design and construction details that occur on a project, questions arise concerning soil conditions and Rock Engineering and Testing Laboratory, Inc. (RETL) (TBPE Firm No. 2101), would be pleased to continue its role as the Geotechnical Engineer during project implementation.

RETL also has great interest in providing materials testing and observation services during the construction phase of this project. If you will advise us of the appropriate time to discuss these engineering services, we will be pleased to meet with you at your convenience.

Sincerely,

lad C Am

Mark C. Rock, P.E. Senior Consultant

ROCK ENGINEERING & TESTING LABORATORY, INC.

Corpus Christi Office: 361.883.4555 Fax: 361.883.4711 6817 Leopard St. Corpus Christi, TX 78409 **San Antonio** Office: 210.495.8000 Fax: 210.495.8015 10856 Vandale San Antonio, TX 78216 **Round Rock** Office: 512.284.8022 Fax: 512.284.7764 7 Roundville Ln. Round Rock, TX 78664

www.rocktesting.com

SUBSURFACE INVESTIGATION, LABORATORY TESTING PROGRAM, AND GEOTECHNICAL RECOMMENDATIONS FOR THE PROPOSED BENEFICIAL USE MITIGATION; PORT OF PORT LAVACA (SWG-2016-01066) CALHOUN COUNTY, TEXAS RETL PROPOSAL NUMBER: CGP031821A (REVISION 3)

RETL REPORT NUMBER: G122209

PREPARED FOR:

BELAIRE ENVIRONMENTAL, INC. P.O. BOX 741 ROCKPORT, TEXAS 78381

MAY 31, 2022

PREPARED BY:

ROCK ENGINEERING AND TESTING LABORATORY, INC. 6817 LEOPARD STREET CORPUS CHRISTI, TEXAS 78409 PHONE: (361) 883-4555; FAX: (361) 883-4711

TEXAS PROFESSIONAL ENGINEERING FIRM NO. 2101

James P. Bauer, P.E. Corpus Christi Branch Manager

Francisco J. Arias, P.E. Senior Project Engineer



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APPENDIX:

Site Vicinity Map Boring and Test Pit Location Plan Boring Logs B-1 to B-9, TR-1 to TR-4 Test Pit logs TP-1 and TP-2 Key to Soil Classification and Symbols Levee Slope Stability Analysis Results Standard Proctor Test Results

INTRODUCTION

This report presents the results of the soil exploration, laboratory testing program, and geotechnical evaluation and recommendations for the proposed Beneficial Use Mitigation; Port of Port Lavaca (SWG-2016-01066) project, located in Calhoun County, Texas. The location of the project is shown on the Site Location Plan included in the Appendix.

The project will include the construction of a Beneficial Use Mitigation Area (BUMA) with a size on the order of approximately 14 acres. The perimeter area of the BUMA will be surrounded by armored and unarmored levees that will provide protection and containment to low and high marsh areas that will be constructed inside the levees under approximately 1 to 3 feet of water.

The levees and marsh areas are planned to be constructed with dredge material currently stockpiled at the Dredged Material Stockpile Area (DMSA). This dredge material will be hauled, dumped and spread by excavation type equipment. Temporary roads will be constructed with caliche base for hauling the dredge material from the DMSA to the BUMA.

The locations of the DMSA and BUMA are shown on the Site Vicinity Map included in the Appendix.

Authorization

The work for this project was performed in accordance with RETL proposal number CGP031821A (Revision 3) dated March 23, 2022. The scope of work and fee was approved by Mr. Charles E. Belaire, President of Belaire Environmental, Inc., by signing our proposal on March 29, 2022. The signed proposal was returned to RETL via e-mail transmission.

Purpose and Scope

The purpose of this exploration was to evaluate the soil and groundwater conditions at the site and to provide geotechnical recommendations for the proposed project. The scope of the exploration and analysis included the subsurface investigation, field and laboratory testing, engineering analysis and evaluation of the subsurface soils, provision of recommendations, and preparation of this report.

The scope of services did not include an environmental assessment. Any statements in this report or on the boring logs, regarding odors, colors, unusual or suspicious items or conditions are strictly for the information of the client.

<u>General</u>

The information submitted for the proposed project is based on details provided by Belaire Environmental, Inc. and the soil information obtained at the boring and test pit locations. If the designers require additional soil parameters to complete the design of the proposed structures for the project, and this information can be obtained from the soil data and laboratory tests performed within the scope of work included in our proposal for this project, RETL will provide the additional information requested as a supplement to this report.

The Geotechnical Engineer states that the findings contained herein have been presented after being prepared in a manner consistent with that level of care and skill ordinarily exercised by reputable members of the Geotechnical Engineer's profession practicing contemporaneously under similar conditions in the locality of the project. RETL operates in general accordance with "*Standard Practice for Minimum Requirements for Agencies Engaged in the Testing and/or Inspection of Soil and Rock as Used in Engineering Design and Construction*", (ASTM D3740). No other representations are expressed or implied, and no warranty or guarantee is included or intended.

This report has been prepared for the exclusive use of Belaire Environmental, Inc. for the specific application for the proposed Beneficial Use Mitigation; Port of Port Lavaca (SWG-2016-01066), located in Calhoun County, Texas.

SITE DESCRIPTION

The project consists of two (2) locations:

- 1. The first location is situated northwest of the intersection of Highway I-35 (Lavaca Bay Causeway) and Dredge Island Road, approximately half a mile southwest of Point Comfort. The BUMA is planned to be constructed at this location.
- 2. The second location (DMSA) is situated approximately 0.3 miles southwest of the Calhoun Port Authority, in an area that has been backfilled with dredge spoils. Soil from this area will be borrowed and used for construction of the BUMA.

The locations of the BUMA and DMSA are shown on the Site Location plan included in the Appendix.

FIELD EXPLORATION

<u>Scope</u>

The field exploration to evaluate the engineering characteristics of the subgrade materials included reconnaissance of the project site, performing the test boring operations, obtaining relatively undisturbed Shelby tube samples from the borings, and collecting samples from test pits.

During the sample recovery operations the soils encountered were classified and recorded on the boring and test pit logs in accordance with "*Standard Guide for Field Logging of Subsurface Exploration of Soil and Rock*", (ASTM D5434).

Nine (9) borings, designated B-1 through B-9, were drilled at the BUMA to depths ranging from 15 to 50 feet, and four (4) borings, designated TR-1 through TR-4, were drilled to a depth of 5 feet along planned temporary roads for the purpose of providing geotechnical recommendations for the project.

In addition, two (2) test pits, designated TP-1 and TP-2, were excavated by others at the DMSA to depths of 10 and 8 feet, respectively, to obtain samples for soil classification and laboratory testing. The tables below provide the boring and test pit identifications, depths and approximate GPS coordinates.

Summary of Boring Information – BUMA										
Boring Identification	Boring Depth (ft)	Location	Approximate GPS Coordinates							
B-1	25	South Levee	N 28.66954° W 96.57270°							
B-2	50	East Levee	N 28.66937° W 96.57126°							
B-3	50	West Levee	N 28.67029° W 96.57323°							
B-4	15	Marsh Area	N 28.67035° W 96.37206°							
B-5	25	East Levee	N 28.67036° W 96.57082°							
B-6	15	Marsh Area	N 28.67082° W 96.57172°							
B-7	25	West Levee	N 28.67160° W 96.57206°							
B-8	50	North Levee	N 28.67122° W 96.57095°							
B-9	15	Marsh Area	N 28.67045° W 96.57239°							

Summary of Boring Information – Temporary Roads									
Boring Identification	Boring Depth (ft)	Location	Approximate GPS Coordinates						
TR-1	5	Temporary Road	N 28.67000 ° W 96.57021 °						
TR-2	5	Temporary Road	N 28.67174 ° W 96.57006 °						
TR-3	5	Temporary Road	N 28.67239 ° W 96.56753 °						
TR-4	5	Temporary Road	N 28.67183 ° W 96.56582 °						

Summary of Test Pit Information – DMSA								
Boring IdentificationTest Pit Depth (ft)LocationApproximate GPS Coordinates								
TP-1	10	DMSA	N 28.64021 ° W 96.55541°					
TP-2	8	DMSA	N 28.63995 ° W 96.55766°					

The number, location and depth of the borings and test pits were defined jointly between RETL and Belaire Environmental. Inc. RETL drilled and logged the borings. The test pits were excavated by others and RETL did the logging and collected the soil samples.

The approximate GPS coordinates for the borings and test pits were obtained using a Garmin GPS model eTrex and are provided in this report and on the boring and test pit logs.

Upon completion of the drilling operations the borings drilled at the BUMA were allowed to collapse and close upon themselves, while the borings drilled for the temporary roads were backfilling with soil cuttings. Boring and Test Pit Location Plans are provided in the Appendix.

The borings performed for this project were used to determine the classification and strengths of the subgrade soils. The information provided on the boring logs includes boring location, boring depth, soil classification, soil strengths, and laboratory test results. The soil samples from the test pits were used to determine soil classification, plasticity and compaction characteristics.

Drilling and Sampling Procedures

The borings at the BUMA were drilled in a marine environment using a drilling rig mounted on a pontoon, while the land-based borings for the temporary roads were drilled with a buggy mounted drilling rig. The drill rigs were equipped with a rotary head turning hollow stem augers to advance the boreholes to the planned depths. Relatively undisturbed soil samples were obtained using thin-wall tube sampling procedures in general accordance with "*Thin Walled Tube Sampling of Soils*", (ASTM D1587). The samples obtained by this procedure were extruded by a hydraulic ram in the field.

The samples were visually classified, placed in plastic bags, marked according to boring number, depth and any other pertinent field data, stored in special containers and delivered to the laboratory for testing.

The test pits were excavated with a backhoe and the soil samples recovered were placed in plastic buckets, sealed, marked according to test pit number, depth and any other pertinent field data, and delivered to the laboratory for testing.

Field Tests and Observations

Water Level Observations – The borings at the BUMA were drilled in a marine environment and the areas were inundated with seawater, while the borings for the temporary roads were land-based. Approximate depths to the mudline measured at the borings for the BUMA and groundwater depths observed at the borehole locations for the temporary roads are discussed in the "<u>Water Depth Observations</u>" section of this report.

Sea Floor and Ground Elevations – Elevations at the boring locations were not provided at the time of this report. Therefore, the depth of water observations in the marine borings are relative to the sea floor (mudline), while the depths noted in the land-based borings and test pits are referenced to the existing ground elevation at the time they were performed.

LABORATORY TESTING PROGRAM

In addition to the field investigation, a laboratory testing program was conducted to determine additional pertinent engineering characteristics of the subsurface materials necessary in analyzing the behavior of the foundation soils at the BUMA and temporary roads areas, and to obtain soil classification and compaction characteristics of the dredge material at the DMSA.

The laboratory testing program on boring samples included supplementary visual classification (ASTM D2487) and water content tests (ASTM D2216). In addition, selected boring samples were subjected to Atterberg limits tests (ASTM D4318) and percent material finer than the #200 sieve tests (ASTM D1140). The shear strengths of selected cohesive soil samples were evaluated from unconfined compressive strength tests (ASTM D2166). The estimated soil strengths were obtained using a hand penetrometer.

The test pit samples were subject to supplementary visual classification (ASTM D2487), water content tests (ASTM D2216), Atterberg limits tests (ASTM D4318) and percent material finer than the #200 sieve. In addition, as requested by the Designer (Lloyd Engineering), one (1) standard Proctor test (ASTM D698) was performed on soil from Test Pit TP-1.

The laboratory testing program was conducted in general accordance with applicable ASTM Specifications. The results of these tests are to be found on the accompanying boring and test pit logs and laboratory testing results provided in the Appendix.

SUBSURFACE CONDITIONS

<u>General</u>

The various types of soils encountered in the test borings and test pits have been visually classified and are described in detail on the boring and test pit logs. The results of the laboratory tests are presented on the boring and test pit logs and in the laboratory test results included in the Appendix. Representative samples of the soils were placed in polyethylene bags and sealed buckets and are now stored in the laboratory for further analysis, if desired. Unless notified to the contrary, the samples will be disposed of three months after issuance of this report.

The stratification of the soil, as shown on the boring and test pit logs, represents the soil conditions at the actual boring and test pit locations to the depths of investigation. Variations may occur and should be expected between and beyond the boring and test pit locations. Lines of demarcation represent the approximate boundary between different soil types, but the transition may be gradual or not clearly defined.

It should be noted that, whereas the borings and test pits were drilled, sampled and logged by experienced drillers, it is sometimes difficult to record changes in stratification within narrow limits. In the absence of foreign substances, it is also difficult to distinguish between discolored soils and clean soil fill.

Soil Conditions

The soils at the BUMA consist mainly of lean clay with some interbedded layers of fat clay, and a few isolated layers of clayey sand. The clayey soils have a firm consistency in the upper 2 feet, with average undrained shear strength (cohesion) on the order of 400 pounds per square foot (psf). The shear strength of the soil increases with depth to values ranging from 1,100 to 3,000 psf (stiff to very stiff consistency).

Along the proposed temporary roads, the soil conditions consist of lean and fat clay with average undrained shear strength is on the order of 2,100 psf.

Finally, the soils observed in the test pits excavated in the DMSA consist of high to very high plasticity fat clays with a soft consistency and sand content ranging from 1 to 19%. It should be noted that a thin (about 3-inch thick) upper crust of soil hardened by desiccation was observed at the top of the test pits. However, underlying this crust the soil is soft, as indicated above.

The tables below provide a summary of the soil properties including soil classification, plasticity limits, fines content and undrained shear strength.

Soil Profile Table – BUMA									
D	Generalized Soil Description	LL	Ы	-#200	Cu	¢	γe	PP	
0-3	CLAYEY Sand, Silty CLAYEY Sand, Fat CLAY with Sand, Sandy Fat CLAY	23-57	10-41	33-85	400		55	0.25-4.0	
3-6	Lean CLAY with Sand, Silty CLAYEY Sand, Fat CLAY with Sand, CLAYEY Sand	25-44	7-26	33-81	1,100		60	0.25-4.5	
6-10	Lean CLAY with Sand, Fat CLAY with Sand			82	2,400		60	2.0-4.5+	
10-23	Lean CLAY , Fat CLAY with Sand, Sandy Lean CLAY , Lean CLAY with Sand	34-48	19-28	65-88	2,900		60	4.0-4.5+	
23-33	Fat CLAY with Sand, Silty CLAYEY Sand, Sandy Lean CLAY, Lean CLAY with Sand, CLAYEY Sand	23-54	5-33	22-85	2,000		60	1.0-4.5+	
33-37	Fat CLAY , Sandy Lean CLAY, SILTY Sand	NP-60	NP-43	34-88	1,500		60	2.0-4.5+	
37-50	Lean CLAY, Sandy Lean CLAY, Fat CLAY with Sand, SILTY Sand, Lean CLAY with Sand, Fat CLAY	NP-67	NP-43	34-100	3,000		60	4.5-4.5+	

Soil Profile Table – Temporary Roads									
D	$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$							PP	
0-3	Fat CLAY , Lean CLAY with Sand	44-64	31-47	83-91	1,700		120	2.5-4.5+	
3-5	Fat CLAY , Fat CLAY with Sand				2,500		120	3.75-4.5+	

Soil Profile Table – Test Pits TP-1 and TP-2								
D	$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$							Qc
0-10	Fat CLAY	55-111	38-81	81-99	<250		110	1-2

Where:

LL = Liquid limit (%) C_u = Soil Cohesion, psf (undrained)

 γ_e = Effective soil unit weight, pcf

PP = Pocket penetrometer resistance (TSF)

Qc = Static cone penetrometer index (TSF)

Exceptions to the above generalized and averaged soil profiles do exist and are shown on the boring and test pit logs included in the Appendix, which provide detailed descriptions of the soils encountered at each location.

Water Depth Observations

As indicated before, approximate water depths at the marine boring locations (B-1 to B-9) at the BUMA are shown in the corresponding boring logs. On the other hand, the borings drilled for the temporary roads (TR-1 to TR-4) and the test pits excavated at the DMSA (TP-1 and TP-2) did not encountered groundwater. However, based on the proximity of these borings and test pits to the shoreline, it is anticipated that groundwater at these locations may be found at depths near the sea water elevation at the adjacent bay.

OSHA Soil Type Classification

The table below provides a summary of the OSHA Soil Type Classification based on the average soil conditions encountered at the project locations.

	OSHA Soil Type Classification – BUMA						
Depth (Feet)	Description	OSHA Soil Type Classification					
0-20	Submerged Soil	Туре С					

OSHA Soil Type Classification – Temporary Roads							
Depth (Feet)	Depth (Feet) Description OSHA Soil Type Classification						
0-5	Cohesive Soil with an Unconfined Compressive Strength Greater between 0.5 and 1.5 TSF	Туре В					

OSHA Soil Type Classification – DMSA						
Depth (Feet)	Description	OSHA Soil Type Classification				
0-10	Cohesive Soil with an Unconfined Compressive Strength less than 0.5 TSF	Туре С				

It should be noted that the information in the tables above considers the average or predominate conditions observed at the corresponding project areas. Soil variations may occur and should be expected within and beyond these areas. The contractor's "competent person" shall make the final determination of the OSHA Soil Type during excavation of the soils at the jobsite areas. If non-cohesive soil or soil from which water is freely seeping is encountered, soils shall be downgraded to Type C soil classification. Slope protection for excavations greater than 20 feet need to be designed and sealed by a Professional Engineer registered in the State of Texas. The maximum allowable slopes during construction for soil OSHA soil types are provided in the following table.

Guidelines for Maximum Allowable Slopes						
Soil or Rock Type Max. Allow. Slopes for Excavations < Than 20' De						
Туре В	1 Horizontal : 1 Vertical					
Туре С	1½ Horizontal : 1 Vertical					

Recommendations for the excavations at the DMSA are beyond our scope of work for this project. The contractor is sole responsible for performing these excavations safely, complying with all applicable local and federal regulations, including OSHA.

GEOTECHNICAL DISCUSSION AND RECOMMENDATIONS

Project Description

As indicated before, the project includes the construction of a Beneficial Use Mitigation Area (BUMA) with a size on the order of approximately 14 acres. The perimeter area of the BUMA will be surrounded by armored and unarmored levees that will provide protection and containment to low and high marsh areas that will be constructed inside the levees under approximately 1 to 3 feet of water. Both levees will be initially constructed to elevation +10.0 feet NAVD 88 (maximum height of 13 feet above mudline) to provide enough free board for construction and to preload the subsoil.

After construction is concluded in the BUMA the levees will be excavated and regraded to lower elevations +5.0 and +2.0 feet NAVD 88, for the armored and unarmored levees, respectively (maximum height of the regraded levees would be 8 feet above mudline). The levees are planned to have 3(H):1 (V) side slopes.

Construction Sequence

The construction activities will start by building the temporary roads to access the BUMA, followed by the construction of the perimeter levees and additional temporary roads at the top of the levees. Once the levees are in place, the interior marsh areas will be constructed and the channels required for water circulation in the marsh areas will be excavated. When construction at the BUMA is concluded the levees will be excavated and regraded, and the temporary roads constructed earlier at the top of the levees will be removed.

The levees are planned to be constructed with dredge material from the DMSA, placed mechanically at the BUMA. Initially, the dredge material will be dumped below 5 to 6 feet of water. After reaching an elevation above sea water, it is recommended to place and compact the dredge material in layers. Additional placement and compaction recommendations for the construction of the levees are discussed in the "Levee Construction" section of the report.

The marsh areas in the BUMA are also planned to be constructed with dredge material from the DMSA. In this case, placement and compaction recommendations for the marsh areas should be provided by the Designer, as factors other than stability and strength (e.g. vegetation growth) will dictate the design of these areas. The final elevations for the low and high marsh areas are +0.5 to +1.65 feet and +2.0 to +3.0 feet NAVD 88, respectively. Considering these elevations, the fill thickness at the marsh areas ranges from 1.5 to 5.0 feet.

The geometry, elevations and dimensions of the structures described herein are shown in Figures 1 and 2 below.

Calhoun County, Texas



Figure 1. Detail of the BUMA.



Figure 2. Cross Section Thru the BUMA.

Considering the type of earth structures and construction sequence planned for the project, the following aspects are addressed in this report:

- 1. Bearing capacity of the foundation soils for the levees and marsh areas.
- 2. Slope stability of the levees.
- 3. Expected settlement and rate of settlement of the levees and marsh areas.
- 4. Pavement analysis and recommendations for the temporary construction roads.
- 5. General construction recommendations.

These topics are further discussed in the following sections of the report.

Soil Bearing Capacity

The calculated ultimate bearing capacity of the foundation soil at the BUMA was estimated to be on the order of **2,000 psf**. Considering that the resulting contact pressure exerted by the levees after attaining its maximum height (13 feet) will be on the order of **1,200 psf**, the resulting Factor of Safety (FS) for bearing capacity will be about **1.7**. After the levees are excavated and regraded to their final heights the contact pressure will reduce to about **660 psf** and the resulting FS will be on the order of **3.0**.

In the marsh areas the maximum contact pressure at mulline elevation is expected to be on the order of 375 psf and the resulting FS for bearing capacity will be approximately **5.0**.

The bearing capacity FS listed above are deemed to be acceptable and hence the subsoil will provide adequate support for the levees and marsh areas at the BUMA.

Slope Stability of the Levees

Slope stability analysis for the levees were performed with the aid of the software SlopeW v. 8.12. SlopeW is a computer program that analyses the stability of slopes utilizing a limit equilibrium approach. The slope stability analysis indicates that the dredge fill material to be placed below water for the construction of the levees should be compacted in such a way to attain a minimum undrained shear strength of **300 psf**, to achieve a minimum FS for slope stability of **1.3** and **1.5**, for short-term and long-term conditions, respectively, which are deemed satisfactory for these structures. The slope stability analysis results are shown graphically in the Appendix.

It should be noted that the designer (Lloyd Engineering) indicated that the stability of the circulation channels is not relevant for the project and that they can be reshaped or reconstructed as necessary. In addition, the final geometry (slope and dimensions) of the channels was unknown at the time of this report. With these considerations, slope stability analysis for the channels was not performed.

Settlement Calculations

Settlement calculations of the subsoil below the levees and the marsh areas in the BUMA were performed with the aid of the software Settle3D v. 2.018. Settle3D is a computer program that calculates stress distribution, elastic (short-term) settlement and consolidation (long-term) settlement of soils subject to loads from foundations and embankments. In addition to the subsoil settlement, the dredge material to be used to construct the levees will also settle under its own weight.

The calculations summarized below are based on the assumption that the maximum height of the levees (13 feet) will be maintained at least for six (6) months to pre-load and consolidate the subsoil, and that the lifetime of this project is 25 years. Different pre-loading times and project lifetimes will result in different results than those summarized in the table below. RETL should be notified if additional analyses for different times are needed, so that we can update our recommendations.

Settlement Analysis Summary								
	Fill Time		Subso	Fill (Drodgo Matorial)				
Structure	Height (feet)	Analyzed	Elastic (Short-Term)	Consolidation (Long-Term)	Total Settlement	Settlement (inches)		
Levee Initial Construction	13	0-6 months	3.0	5½	81⁄2	4¾		
Levee Regraded	8	6 months to 25 years	1/4	1.0	1¼	1.0		
Marsh Area	5	0-25 years	11⁄2	3¾	5¼	1¾		

The following conclusions can be derived from the table above:

- 1. The subsoil below the levees, when loaded with the maximum levee embankment height of 13 feet during the 6-month preloading period, will experience approximately 3.0 and $5\frac{1}{2}$ inches of elastic and consolidation settlement, respectively, which in turn will produce a total settlement of the subsoil of about $3.0 + 5\frac{1}{2} = 8\frac{1}{2}$ inches. In addition, the body of the levees will experience a settlement on the order of $4\frac{3}{4}$ inches. Considering the settlement of the subsoil and the settlement of the levees, the anticipated settlement at the top of the levees would be on the order of $8\frac{1}{2} + 4\frac{3}{4} = 13\frac{1}{4}$ inches.
- 2. After the pre-loading period the levees are planned to be excavated and regraded to their final elevations. The <u>additional</u> total settlement of the subsoil after the levees are regraded is approximately $1\frac{1}{4}$ inches. In addition, the body of the levees will experience a settlement on the order of 1.0 inch. Considering the settlement of the subsoil and the settlement of the levees, the anticipated settlement at the top of the regraded levees would be on the order of $1\frac{1}{4} + 1.0 = 2\frac{1}{4}$ inches.
3. The subsoil below the marsh areas, when loaded with the maximum fill height of 5 feet, will experience approximately $1\frac{1}{2}$ and $3\frac{3}{4}$ inches of elastic and consolidation settlement, respectively, which in turn will produce a total settlement of the subsoil of about $1\frac{1}{2}$ + $3\frac{3}{4}$ = $5\frac{1}{4}$ inches. In addition, the body of the dredge fill material will experience a settlement on the order of $1\frac{3}{4}$ inches. Considering the settlement of the subsoil and the settlement of the fill, the anticipated settlement at the top of the marsh areas would be on the order of $5\frac{1}{4} + 1\frac{3}{4} = 7.0$ inches.

The estimated settlements indicated above should be considered when planning the final elevations of the levees and marsh areas, and the amount of dredge material required for their construction. We also recommend that the contractor monitors settlement of the levees and marsh areas and that this settlement monitoring information is provided to RETL, so that we can adjust our recommendations, if required.

Unsurfaced Aggregate Pavement Recommendations

It is understood that temporary roads will be installed for heavy truck traffic allowing the transportation of material from the DMSA to the BUMA. The temporary roads are anticipated to be unsurfaced and constructed using a caliche base material. The location of the temporary roads is shown on the Figure 1 in the "Geotechnical Discussion and Recommendations" sections of the report.

In addition, similar roads will be constructed atop the levees to allow for construction of the levees and marsh areas. These temporary roads will be eventually removed when the levees are excavated and regraded to their final planned elevation.

Unsurfaced pavements with exposed aggregate (in this case caliche base material) are typically able to be and required to be bladed, graded, maintained and/or repaired throughout their life and are therefore typically not designed as structurally equivalent to flexible asphalt pavements carrying the same or similar traffic.

Unsurfaced Aggregate Pavement	Option 1	Option 2
Caliche Base Material	24 inches	24 inches
Tensar Geogrid TX-5	Yes	
Lime Stabilized Subgrade (6%)		8 inches
Compacted Subgrade	12 inches	

The recommended pavement sections are summarized in the table below:

The pavement section recommended above is preliminary and should be confirmed after additional information regarding the expected traffic (type of vehicles, weight, frequency, ESALs, etc.) and regarding the proposed caliche base material (CBR, plasticity, fines content, etc.) is provided by the client and reviewed by RETL. This information should be transmitted to RETL as soon as it becomes available, so that we can review the pavement recommendations provided herein and revise it, if warranted.

The caliche base material to be used for the unsurfaced aggregate pavement should be placed in maximum 8-inch thick loose lifts and compacted to a minimum density of 98 percent of the maximum dry density as determined by the modified Proctor test (ASTM D1557) and within \pm 1.5 percent of the optimum moisture content.

Pavement Subgrade Preparation

In inland areas where the temporary road pavements will be constructed, after all surface organics and deleterious materials have been removed to the desired subgrade elevation, the subgrade shall be proofrolled using a heavy pneumatic roller. Any soft areas identified shall be removed to firm soils, reworked and recompacted in place to obtain a stable and nonyielding subgrade. If required, a "bridging layer" may be constructed at the bottom of the exposed subgrade by placing 8 inches of "#57 stone", compacted with several passes of heavy construction equipment weighting at least 20 tons to achieve "ordinary compaction", as defined by TxDOT Item 132 Standard Specification. This bridging layer should provide a more stable subgrade surface and will facilitate subsequent fill placement. A layer of filter fabric meeting TxDOT DMS-6200 Specification (Type 1 or 2) should be place atop the #57 stone to separate this open-graded aggregate from the fill to be placed above.

Temporary inland pavements may be constructed using either Option 1 or Option 2 sections listed in the table above, while temporary levee pavements may be constructed using Option 1 section listed in the table.

Upon completion of the proofrolling, and if an Option 1 pavement section will be used, the subgrade soils should be scarified, moisture conditioned and compacted to the minimum specified depth of 12 inches. The subgrade should be compacted to a minimum of 95 percent of the maximum dry density, as determined by the standard Proctor (ASTM D698) at or above the optimum moisture content. After proper compaction of the subgrade, the specified geogrid shall be placed on the properly prepared raw subgrade in accordance with the manufacturer's recommendations.

Upon completion of the proofrolling, and if an Option 2 pavement section will be used, the lime stabilization operations shall be performed in accordance with TxDOT Item 260, *"Lime Treatment For Materials Used As Subgrade (Road Mixed)."* Based on the results of the Atterberg limits tests for the subgrade soils and associated curves provided in TxDOT Test Method 121-E, RETL recommends that the lime be mixed at the rate of 6 percent, based on the maximum dry unit weight of the raw subgrade soils as determined by the standard Proctor test (ASTM D698). The lime stabilized soils should be compacted to a minimum density of 98 percent of the maximum dry density, as determined by a standard Proctor test (ASTM D698), at or above the optimum moisture content.

Drainage and Maintenance of Pavement Systems

The pavement sections provided in this report are designed based on pavement sections constructed on similar subgrade soils and for facilities similar to those planned for construction at this site. Allowances for proper drainage and proper material selection of base materials are most important for performance of pavements. Ruts, birdbaths and poor site drainage allow for quick deterioration of the pavement primarily due to saturation of the base materials and/or subgrade soils.

Unsurfaced aggregate pavements generally require very dedicated and frequent maintenance as they are exposed directly to the elements with little to no confinement of the surficial aggregate. Without proper maintenance, moisture infiltration into the base material and subgrade will result in rapid deterioration of the pavement system. RETL recommends that the owner protect their investment by incorporating an aggressive maintenance program.

CONSTRUCTION CONSIDERATIONS

Site Preparation

In the inland areas where the temporary roads are planned, clearing and grubbing operations should be performed to excavate and remove organics, roots, rubble, deleterious matter, and any other unsuitable materials, to a minimum depth of six (6) inches, or deeper if needed for their complete removal. This excavation should extend laterally at least 3 feet beyond the footprint of the temporary road structures. The excavated material should not be used for construction.

Once the clearing and grubbing operations are concluded, the subgrade should be prepared as indicated in the "**Pavement Subgrade Preparation**" section of the report.

Levee Construction

As indicated before, the levees are planned to be constructed with dredge material borrowed from the DMSA. This material consists of fat clays with very high plasticity and limited sand contents varying from 1 to 19 percent. This material, when excavated and transported to the BUMA, is anticipated to arrive in a blocky shape. In other words, large pieces (chunks) of clay will be excavated from the DMSA and will arrive to the DMSA in a similar shape.

The initial construction of the levees will consist of dumping the dredge material under about 5 or 6 feet of water, to build the base of the levees. Placement of this material in layers and compacting it under water, considering the blocky shape of the clay indicated above, might be challenging. The contractor should adjust his construction procedures and utilize construction equipment capable of placing and compacting the dredge fill material in a controlled engineered fashion, to result in an undrained shear strength of the fill placed below water of at least 300 psf, to provide a stable fill embankment, as previously discussed in the "**Slope Stability of the Levees**" section of the report.

Once the levee sections are above water, we recommend performing cone penetrometer testing (CPT) to confirm that the fill placed below water is competent and reached the minimum undrained shear strength indicated above, before placing additional fill. RETL should be contacted to coordinate CPT testing.

Additional fill above water to build the levees should be placed in no greater than 8-inch thick loose lifts and then compacted to a minimum density of 95 percent of the maximum dry density, as determined by the standard Proctor test (ASTM D698), and at or above the optimum moisture content. Refer to the compaction test results included in the Appendix.

Earthwork and Acceptance

Exposure to the environment may weaken the soils at the pavement bearing level if the excavations remain open for long periods of time. Therefore, it is recommended that the pavement excavations be extended to final grade and that the pavements be constructed as soon as possible to minimize potential damage to the bearing soils.

The pavement bearing subgrade should be free of loose soil, ponded water or debris and should be observed prior to placing pavement constituents by the Geotechnical Engineer or his designated representative.

Pavement constituents should not be placed on soils that have been disturbed by rainfall or seepage. If the bearing soils are softened by surface water intrusion or by desiccation, the unsuitable soils must be removed from the pavement excavations and be replaced with properly compacted "<u>Select Fill</u>" prior to placement of pavement constituents per Engineer's direction.

The Geotechnical Engineer or his designated representative should monitor subgrade preparation and placement of fill. As a guideline, a minimum of one in-place density test shall be performed on the subgrade soils and each subsequent lift of fill for each 3,000 square feet, or a minimum of three in-place density tests per testing interval, whichever is greater. Any areas not meeting the required compaction should be recompacted and retested until compliance is met.

Dredge Fill Material

Dredge fill material for the construction of the levees and marsh areas should be free of roots, organics, trash, debris, deleterious materials and otherwise unsuitable soil.

It should be noted that levees constructed with highly plastic soils are prone to experience swell and shrinkage movements related to moisture content variations caused by evaporation, rainfall, temporal humidity variations and change in water level, potentially resulting on differential settlement and fissures of the levee faces that should be promptly repaired.

Select Fill

Imported select fill for this project should be homogenous, free from organics and other deleterious materials and should have a maximum liquid limit of 40 percent and a plasticity index (PI) between 7 and 18. The select fill soils shall have a minimum of 35 percent passing the #200 sieve and no soil particles exceeding 1½ inches will be permitted. The select fill should be placed in no greater than 8-inch thick loose lifts and then compacted to a minimum density of 95 percent of the maximum dry density, as determined by the standard Proctor test (ASTM D698), and at or above the optimum moisture content.

GENERAL COMMENTS

If significant changes are made in the character or location of the proposed project, a consultation should be arranged to review any changes with respect to the prevailing soil conditions or the recommendations presented herewith At that time, it may be necessary to submit supplementary recommendations.

It is recommended that the services of RETL be engaged to test and evaluate the soils in the pavement excavations prior to placement of pavement constituents in order to verify that the bearing soils are consistent with those encountered in the borings. RETL cannot accept any responsibility for any conditions that deviate from those described in this report, nor for the performance of the project if not engaged to also provide construction observation and testing. If it is required for RETL to accept any liability, then RETL must agree with the plans and perform such observation during construction as we recommend.

All dewatering, sheeting, shoring, and bracing of trenches and excavations should be made the responsibility of the contractor and should comply with all current and applicable local, state and federal safety codes, regulations and practices, including the Occupational Safety and Health Administration.

APPENDIX



- GEOTECHNICAL ENGINEERING
- CONSTRUCTION MATERIALS ENGINEERING & TESTING
- SOILS ASPHALT CONCRETE

SITE VICINITY MAP



May 31, 2022 Attn: Ms. Laura Fox RETL Job Number G122209 BENEFICIAL USE MITIGATION (SWG-2016-01066) Port of Port Lavaca Calhoun County, Texas

ROCK ENGINEERING & TESTING LABORATORY, INC.

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San Antonio

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- GEOTECHNICAL ENGINEERING
- CONSTRUCTION MATERIALS ENGINEERING & TESTING
- SOILS ASPHALT CONCRETE

BORING LOCATION PLAN – MITIGATION AREA



May 31, 2022 Attn: Ms. Laura Fox RETL Job Number G122209 BENEFICIAL USE MITIGATION (SWG-2016-01066) Port of Port Lavaca Calhoun County, Texas

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- GEOTECHNICAL ENGINEERING
- CONSTRUCTION MATERIALS
 ENGINEERING & TESTING
- SOILS ASPHALT CONCRETE

TEST PIT LOCATION PLAN – (DMSA)



May 31, 2022 Attn: Ms. Laura Fox RETL Job Number G122209 BENEFICIAL USE MITIGATION (SWG-2016-01066) Port of Port Lavaca Calhoun County, Texas

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APPENDIX

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		SH		D- 0.25	25	22	12	10			22	CLAYEY SAND dark gray moist soft (SC)
		S-1	_	F= 0.25 					+			(3% gravel sized particles) (65% sand particles)
	- 5 -	SH S-2		P= 4.5	21	44	18	26			81	LEAN CLAY WITH SAND, with aggregate, gray, moist, very stiff (CL)
		SH		P= 4.5+	14							Same as above, brown and gray.
		5-3 SH										
	- 10 -	S-4		P= 4.5+ 	17 		<u> </u>		<u> </u>			Same as above, gray.
		SH S-5		P= 4.5+	14	34	15	19			88	LEAN CLAY, gray, moist, very stiff. (CL)
		SH		P= 4 5+	18							Same as above.
	- 15 -	S-6		1 4.0								
			-				+		+			
		SH		P= 4.5+	24							FAT CLAY WITH SAND, greenish gray, moist, very stiff. (CH)
	- 20 -		Π									
	- 25 -	SH S-8		P= 4.5+	25	54	21	33			85	Same as above, gray and brown. (CH)
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	X : {	II			rpus C	hristi,	Texas	7840	9			LOCATION: Calhoun County, Texas
	ABORAT		21	ORATE Tel Fax	ephon <: 361	ie: 36 -883-4	1-883- 1711	4555				NUMBER: G122209
	~											DATE(S) DRILLED: 4/19/2022
	FIE)A ⁻	ΓA		LABO	DRAT	OR	Y DAT	A		DRILLING METHOD(S):
						AT	TERB	ERG				Hollow Stem Auger
					(%)			S	-		(%)	
		~			ENT						EVE	Mudline was approximately 2 feet below water surface
		1BEF			ONT	⊥₩	IWI	≚		E (1S 00	
ABO	Ē	NN	s s	SQ F SQ F SQ F SQ F	SE C		TIC	TICI	VSIT	ESSIN TH Q FT	0. 2(
SYI	TH (IPLE	IPLE	SNO'	STUI	nal-	PLAS	PLAS	DEN	APRE ENG VS/S	N SU	SURFACE ELEVATION: N/A
SOIL	DEP	SAN	SAN		MO	LL	PL	PI	POL	CON STR (TON	MIM	DESCRIPTION OF STRATUM
		<u>е</u> ц										
		S-1		P= 1.5	26						38	SILTY CLATEY SAND, dark gray, moist, iirm.
		SH		P= 0.25	26	25	18	7			45	Same as above, gray, soft. (SC-SM)
	- 5 -	SH	-				+		+	+		
		S-3		P= 2.0	23				101	2.1	82	LEAN CLAT WITH SAND, gray, moist, very sun.
		SH		P= 4.5+	23							Same as above.
	- 10 -	SH	-						+	+		LEAN CLAX brown and gray major yory stiff (CL)
		S-5		P= 4.0	22	48	20	28			88	LEAN CLAT , brown and gray, moist, very suit. (CE)
		SH		P= 4.5+	16							Same as above.
	- 15 -											
		SH S-7		P= 4.5+	22							Same as above.
	20											
							+		+			
		SH S-8		P= 1.0	23	23	18	5	113	0.8	22	SILTY CLAYEY SAND, brown, moist, firm. (SC-SM)
		-										
		1							+	+		
		SH S-9		P= 2.0	32						82	LEAN CLAY WITH SAND, brown and gray, moist, stiff.
		-										
									+	+		
	- 35 -	SH S-10		P= 4.5	23	60	17	43			88	FAT CLAY, brown and gray, moist, very stiff. (CH)
		1							+	+		
		SH S-11		P= 4.5+	16							LEAN CLAY, gray and brown, moist, very stiff.
		-										
		1							+			
	45	SH S-12	2	P= 4.5+	24							FAT CLAY WITH SAND, gray and brown, moist, very stiff.
												Boring was terminated at a depth of 45 feet.
, er												
2220												
و و												
	N - ST		ער		TRA		TES		SIST			REMARKS:
5	Qc - S	TAT	IC	CONE PE	NET	RON	1ETE	RTE	EST IN	NDEX		Drilling operations were performed by On Point Geophysical at GPS Coordinates N 28.66937° W 96.57126°
	P - PC	CKI	ΕT	PENETR	DME	TER	RES	ISTA	NCE			
·												

									LU	GU	. D(JRING D-3 SHEET 1 of 1
	Neiner Reiner			Roo 681 Col Tel Fay	ck Eng 17 Lec rpus C ephon (: 361	gineeri pard S Christi, ne: 36 -883-4	ng & 1 Street Texas 1-883- 1711	Festing 7840 4555	g Lab. I 9	nc		CLIENT: Belaire Environmental, Inc. PROJECT: Port of Port Lavaca (SWG-2016-01066) LOCATION: Calhoun County, Texas NUMBER: G122209
												DATE(S) DRILLED: 4/21/2022 - 4/22/2022
	FIE		A	TA			DRAT	OR)	/ DAT	A	1	DRILLING METHOD(S): Hollow Stem Auger
					()			erg S				
NL SYMBOL	ЕРТН (FT)	MPLE NUMBER	MPLES	BLOWS/FT TONS/SQ FT TONS/SQ FT : TONS/SQ FT	DISTURE CONTENT (9	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	KY DENSITY JUNDS/CU.FT	MPRESSIVE RENGTH DNS/SQ FT)	NUS NO. 200 SIEVE (%	GROUNDWATER INFORMATION: Mudline was approximately 5 feet below water surface SURFACE ELEVATION: N/A
0 S	DE	SA SA	\S V	/ żä≓ð	Ĕ	LL	PL	PI	PC PC	ST CC	Σ	DESCRIPTION OF STRATUM
		SH S-1		P= 0.25	42	41	11	30			44	CLAYEY SAND, dark gray, moist, soft. (SC) (10% gravel sized particles) (45% sand particles)
	- 5 -	SH S-2		P= 4.0	23							LEAN CLAY WITH SAND, gray, moist, very stiff.
		SH S-3		P= 4.5	20							Same as above, brown and gray.
		SH S-4		P= 4.5+	20							Same as above.
	- 10 -	SH S-5		P= 4.5+	18							Same as above.
	 	SH		 P= 4.5+	15	39	16	23		F	65	SANDY LEAN CLAY, brown, moist, very stiff. (CL)
	 - 20 -	SH S-7		P= 4.5+	16							Same as above, gray and brown.
	 - 25 - 	- SH - S-8		P= 4.5+	20							Same as above.
		SH S-9		P= 4.5	22							Same as above.
	 - 35 - 	SH S-10		P= 4.5+	15							Same as above.
	- 40 - - 40 -	SH S-11		P= 4.5	20		 			 	 	Same as above.
	 - 45 - 	SH S-12		P= 0.25	24	NP	NP	NP			34	SILTY SAND, brown, moist, soft. (SM) (66% sand particles)
				P=45	24	67	24	12			100	FAT CLAY, brown and greenish gray, moist, very stiff. (CH)
	- 50 -	S-13		1 = 4.0	24		24				100	Boring was terminated at a depth of 50 feet.
	N - S1 Qc - S P - PC		⊢ IC ET	RD PENE CONE PE	TRA ENET	L TION TROM TER	TES IETE RES	T RE R TE ISTA	SIST ST IN NCE	ANCE		REMARKS: Drilling operations were performed by Clean Harbor at GPS Coordinates N 28.670290° W 96.573231°

									LO	g of	B	ORING B-4 SHEET 1 of 1
		NG &	~									CLIENT: Belaire Environmental, Inc.
	NEINEER		ES	Roc 681	ck Eng	gineeri	ing & 1 Street	resting	g Lab. I	nc		PROJECT: Port of Port Lavaca (SWG-2016-01066)
		IIH		Col	rpus C	hristi,	Texas	7840	9			LOCATION: Calhoun County, Texas
	ABORAT		AP	Fax Fax	ephon <: 361	e: 36 -883-4	1-883- 1711	4555				NUMBER: G122209
	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	SA IN										DATE(S) DRILLED: 4/21/2022
	FIE	LD D	A	Ā		LABO	DRAT	OR	DAT	A		DRILLING METHOD(S):
						AT	TERB	ERG				Hollow Stem Auger
					(%)			×	-		(%)	GROUNDWATER INFORMATION:
							⊢	NDE			IEVE	Mudline was approximately 5 feet below water surface
_		MBE			NO	MIT	LIMI	μ	ᠵᄩ		00 S	
MBO	Ê	NN	S	S/FT SQ F SQ F SQ F	RE 0		STIC	STIC	NSIT S/CU	ESSI TH Q F	10. 2	
SΥ	TH (	APLE	1PLE	NONS/	STU	LIQU	PLAS	PLA8	NDS	APRE ENG NS/S	US N	SURFACE ELEVATION: N/A
soll	DEP	SAN	SAN/	анн хано	MO	LL	PL	PI	POL	STR TOI	MIN	DESCRIPTION OF STRATUM
		SH		D- 0.25	12	42	15	27			46	CLAYEY SAND dark gray moist (SC)
		S-1		P= 0.25 	43	42			<u> </u>		40	(2% gravel sized particles) (51% sand particles)
	5	_ SH _ S-2		P= 3.0	25				99	0.6		LEAN CLAY WITH SAND, gray, moist, firm.
		SH		P= 4.25	21							Same as above, brown and gray.
		- SH S-4		P= 4.5	19							Same as above.
		SH		P= 4.5	22							Same as above.
		SH		D- 1 5+	18							Same as above.
	15	_ S-6		1 = 4.51	10							Boring was terminated at a depth of 15 feet.
24												
5/13/2												
TO												
EI.												
Х												
J R(												
09.GF												
G1222												
DRING	N 0-										I	REMARKS:
F_B(	QC - S	STAT	IC	CONE PE	i RA ENET	RON	IES IETE	R TE	SIST IN			Drilling operations were performed by Clean Harbor at GPS Coordinates
000	P - P(	OCKE	ΞT	PENETR	OME	TER	RES	ISTA	NCE			
Ц												

										<u>G OF</u>	B	CRING B-3 SHEET 1 of 1
	NGINEERI No AFIO		A the G	Roc 681 Con Tel Fax	ck Eng 7 Leo pus C ephon c: 361	jineerii pard S hristi, e: 36 ⁻ -883-4	ng & T Street Texas 1-883-4 711	esting 7840 4555	g Lab. Ii 9	nc		CLIENT: Belaire Environmental, Inc. PROJECT: Port of Port Lavaca (SWG-2016-01066) LOCATION: Calhoun County, Texas NUMBER: G122209 DATE(C) DBILLED: 4/21/2022
				- ^		A D C	<u> </u>	· `		· ^		
$\left  \right $	FIE		ΓA	A		_ABC				A		Hollow Stem Auger
SOIL SYMBOL	<b>DEPTH (FT)</b>	SAMPLE NUMBER	SAMPLES	N: BLOWS/FT P: TONS/SQ FT T: TONS/SQ FT QC: TONS/SQ FT	MOISTURE CONTENT (%)				DRY DENSITY POUNDS/CU.FT	COMPRESSIVE STRENGTH (TONS/SQ FT)	MINUS NO. 200 SIEVE (%)	GROUNDWATER INFORMATION: Mudline was approximately 6 feet below water surface SURFACE ELEVATION: N/A DESCRIPTION OF STRATUM
		SH		P= 3 75	22	57	16	41	103	26	85	FAT CLAY WITH SAND, brown and gray, moist, very stiff.
		S-1 SH		D- 2 75	27	01	10	- 1	100	2.0	00	(CH) Same as above, grav.
	- 5 -	S-2 SH		P-125	21							Same as above.
		S-3 SH		P= 3 75	22				86	13		Same as above, stiff.
	- 10 -	S-4 SH		P = 0.75 	 12							I FAN CLAY WITH SAND gray and brown moist very stiff
		S-5		P= 4.5+	13							Same as above, gray and dark brown
	- 15 -	S-6		P= 4.5+	18							Same as above, gray and dark brown.
	  - 20 -	SH S-7		P= 4.5+	21							Same as above.
	  - 25 -	SH S-8		P= 4.5+	24							Same as above.
NG G122209.GPJ ROCK_ETL.GDT 5/13/22												
LOG_OF_BOR	N - ST Qc - S P - PC	TANE TAT DCKE	DAF IC ET	rd Pene ⁻ Cone Pe Penetro	TRAT NET	TION ROM TER	TES IETE RESI	T RE R TE STA	SIST ST IN NCE	ANCE IDEX		REMARKS: Drilling operations were performed by Clean Harbor at GPS Coordinates N 28.670359° W 96.570815°

									LO	G OF	B	ORING B-6 SHEET 1 of 1
	6	NG &	$\overline{\times}$									CLIENT: Belaire Environmental, Inc.
	NGINEER		ES	Ro 68	ck Eng 17 Leo	gineeri pard S	ng & 1 Street	resting	g Lab. I	nc		PROJECT: Port of Port Lavaca (SWG-2016-01066)
$ \langle$					rpus C	hristi,	Texas	7840 4555	9			LOCATION: Calhoun County, Texas
	PRATO		CORP	OBAN Fax	c: 361	-883-4	1-000-	-000				NUMBER: G122209
			~		1							DATE(S) DRILLED: 4/21/2022
	FIE	LD D	DAT	ΓA		LABC	ORAT	OR	′ DAT	A		
						AT		ERG S			_	TONOW Stell Auger
					Т (%			X	1		E (%)	GROUNDWATER INFORMATION:
		L L L			ITEN		μ	IND			SIEV	Mudline was approximately 5 feet below water surface
Ъ		JMBI		- 타타면	CO			L \	Υ.FT	SIVE T	200	
YMB	H (FT	Ž Щ	В	WS/F S/SQ S/SQ VS/S(	URE	an	ASTIC	ASTIC	ENSI DS/C	RESS IGTH /SQ F	NO	
OIL S	EPT	AMPI	AMPL	DNO 10N 10N 10N	OIST		Ę	4		DMP TREN ONS	SUNI	SURFACE ELEVATION: N/A
S S		\$	\@	/ ≍ŭ≓ð	Σ		PL	PI		5 S F	Σ	DESCRIPTION OF STRATUM
		SH S-1		P= 0.25	34	38	11	27			38	<u><b>CLAYEY SAND</b></u> , dark gray, moist, very soft. (SC) (1% gravel sized particles) (61% sand particles)
	- 5	SH S-2		P= 3.0	19				110	1.9		LEAN CLAY WITH SAND, gray, moist, stiff.
		SH S-3		P= 4.5	17							Same as above, gray and brown, very stiff.
		SH S-4		P= 4.25	23							Same as above.
		SH S-5		P= 4.5	15							Same as above, dark brown and gray.
				D- 1 5+	20							Same as above, brown and grav,
	15	S-6		1 - 4.01	20							Boring was terminated at a depth of 15 feet.
4												
0.00												
777 0 0												
	, N - S1			RD PENE	TRA	TION	TES	TRE	SIST	ANCE		REMARKS:
5	Qc - S P - PC	STAT DCKI	IC ET	CONE PE PENETRO	ENET OME	RON TER	IETE RES	R TE	ST IN	IDEX		Drilling operations were performed by Clean Harbor at GPS Coordinates N 28.67082° W 96.57172°

									LO	<u>g of</u>	- B(	ORING B-7 SHEET 1 of 1
	Neuren Park		A PL	Ron 681 Col Col Tel Fax	ck Eng I7 Leo rpus C ephon (: 361	jineeri pard S hristi, e: 36 ⁻ -883-4	ng & T Street Texas 1-883- 1711	esting 7840 4555	g Lab. Ii 9	nc		CLIENT: Belaire Environmental, Inc. PROJECT: Port of Port Lavaca (SWG-2016-01066) LOCATION: Calhoun County, Texas NUMBER: G122209
			~									DATE(S) DRILLED: 4/21/2022
	FIE					_ABC			/ DAT	A		DRILLING METHOD(S): Hollow Stem Auger
OIL SYMBOL	ЕРТН (FT)	AMPLE NUMBER	AMPLES	BLOWS/FT TONS/SQ FT CONS/SQ FT CONS/SQ FT	OISTURE CONTENT (%)	: LIQUID LIMIT		PLASTICITY INDEX	RY DENSITY DUNDS/CU.FT	OMPRESSIVE TRENGTH ONS/SQ FT)	INUS NO. 200 SIEVE (%)	GROUNDWATER INFORMATION: Mudline was approximately 5 feet below water surface SURFACE ELEVATION: N/A
S		SH	\vi		Σ		PL	PI			Σ	DESCRIPTION OF STRATUM
		S-1		P= 2.75	23	55 	17 	38 	101	0.8	65	SANDT FAT CLAT, dark gray, moist, mm. (CH)
	- 5 -	S-2		P= 4.25	15							<u>LEAN CLAT WITH SAND</u> , gray and brown, moist, very stin.
		S-3 SH		P= 4.5	20							Same as above.
	- 10 -	S-4		P= 4.5+	14							Same as above
		S-5 SH		P= 4.5+	17							Same as above, dark brown
	- 15 -	S-6		P= 4.5+	17							
	 - 20 -	SH S-7		P= 4.5+	18							Same as above.
	  - 25 -	SH S-8		P= 4.5+	24							Same as above, brown and gray.
	N - ST Qc - S P - PC	ANE TAT CKI	DAI TIC ET	RD PENE CONE PE PENETR(	TRAT ENET OME	FION ROM TER	TES IETE RES	T RE R TE ISTA	SIST ST IN NCE	ANCE IDEX		KEMARKS: Drilling operations were performed by Clean Harbor at GPS Coordinates N 28.671602° W 96.572060°

			CRING D-0 SHEET 1 OF 1
ENGINE FUEL FOR THE FOR	ck Engineering & Tes 17 Leopard Street rpus Christi, Texas 7 ephone: 361-883-45 (; 361-883-471	sting Lab. Inc 8409 555	CLIENT:Belaire Environmental, Inc.PROJECT:Port of Port Lavaca (SWG-2016-01066)LOCATION:Calhoun County, TexasNUMBER:G122209
NCAL INCOM			DATE(S) DRILLED: 4/21/2022
FIELD DATA	LABORATC	DRY DATA	DRILLING METHOD(S):
	ATTERBER	RG	Hollow Stem Auger
MBOL (FT) E NUMBER SS SSQ FT SSQ FT SSQ FT	IRE CONTENT (%)	STICITY INDEX NSITY S/CU.FT S/CU.FT S/CU.FT S/IN S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.FT S/CU.	GROUNDWATER INFORMATION: Mudline was approximately 5 feet below water surface
PTH - PTH - NULE	DLA	PLA: V DE MPRI MPRI NNS/S	SURFACE ELEVATION: N/A
SAN SAI	≥ LL PL	MIN CO DR	DESCRIPTION OF STRATUM
SH S-1 P= 4.0	25		FAT CLAY WITH SAND, gray and brown, moist, very stiff.
SH 5 S-2 P= 3.5	22	105 1.5	LEAN CLAY WITH SAND, gray and brown, moist, very stiff.
SH S-3 P= 4.5	20		Same as above.
SH S-4 P= 4.0	20		Same as above.
SH S-5 P= 4.25	23		Same as above.
SH 15 S-6 P= 4.5	21		Same as above, dark brown and gray.
S-7 P= 4.25	20		Same as above.
SH 25 5-8 P= 3.5	21		<b>CLAYEY SAND</b> , brown and gray, moist, very stiff.
SH 30 - SH S-9 P= 4.5+	17		Same as above, gray.
SH - 35 - S-10 ■ P= 2.0	22 NP NP 1	NP 94 0.6 34	SILTY SAND, gray and brown, moist, stiff. (SM) (66% sand particles)
CC/EVG L 40 - SH S-11 P= 4.5	25		FAT CLAY WITH SAND, gray and brown, moist, very stiff.
SH 45 S-12 P= 4.5	15		<b>LEAN CLAY WITH SAND</b> , gray and brown, moist very stiff.
G1960222 50 SH P= 4.5	16		Same as above, gray.
			Boring was terminated at a depth of 50 feet.
N - STANDARD PENE Control Control Penel Control Control Penel P - POCKET PENETRO	TRATION TEST NETROMETER OMETER RESIS	RESISTANCE TEST INDEX TANCE	REMARKS: Drilling operations were performed by Clean Harbor at GPS Coordinates N 28.671224° W 96.570952°

											• B(	<b>PRING B-9</b> SHEET 1 of 1
	LER.	ING &	TE	N Ro	ck End	ineeri	na & T	esting	ılah l	nc		CLIENT: Belaire Environmental, Inc.
	NGINE			681	17 Leo	pard S	Street	esun	j Lab. I			LOCATION: Calbour County Toxon
					rpus C ephon	hristi, e: 36	Texas 1-883-	7840 4555	9			NUMPER: C10000
	RATO	R IN	CORP	Fax	c' 361	-883-4	711					
		$\sim$										DATE(S) DRILLED: 4/21/2022
	FIE		DAT	A			DRAT	OR	/ DAT	A		Hollow Stem Auger
					_			ERG S				······
					Τ (%			X			Е (%	GROUNDWATER INFORMATION:
		Ľ.			TEN		⊨	D			SIEV	Mudline was approximately 5 feet below water surface
		MBE			NOC	TIMI	LIM	È	ᠵᄪ	⊒ ⊊	5003	
MBC	Ē		ŝ	'S/F1 /SQ I /SQ I /SQ I S/SQ	IRE		STIC	STIC	NSIJ S/CL	ESS STH SQ F	Q.	
ΓS	TH	APLE	APLE		ISTL	LIQL	PLA	PLA	ND ND	VIPR KENC NS/S	US I	SURFACE ELEVATION: N/A
sol	DEF	SAN	SA/	Z L L O	οM	LL	PL	ΡI	POL	STF STF TO	ΝΨ	DESCRIPTION OF STRATUM
	-	SH		P= 0.75	59	105	36	69			70	<b>FAT CLAY WITH SAND</b> , dark gray, moist, soft. (CH)
		_ 」 sн			+			·				(0.4% gravel sized particles) (30% sand particles)
	- 5	_ S-2		P= 0.25 	25				L		33	
		SH S-3		P= 4.5+	21							LEAN CLAY WITH SAND, gray, moist, very stiff.
	- 10	_ SH _ S-4		P= 4.5+	17							Same as above, gray and brown.
		SH S-5		P= 4.5+	18							Same as above, gray and dark brown.
	1	SH		P= 4.5+	21							Same as above.
	- 15	]										Boring was terminated at a depth of 15 feet.
N												
/13/2												
DT 5												
J.G												
Я												
J RO												
09.GP												
G1222(												
RING	]											REMARKS:
BB	N - S	ΙΑΝΕ Stat	Jaf IC			⊓ON 'ROM	IES 1FTF	I RE R TF	SIST.			Drilling operations were performed by Clean Harbor at GPS Coordinates
000	P - P(	CKI	ΞT	PENETRO	OME	TER	RES	ISTA	NCE			IN 20.070440 VV 90.372391
Ч <b>—</b>												

										<u>, OL</u>	<u>BO</u>	KING IR-1 SHEET 1 of 1
	HEALER PROPERTY IN		A CORP	Roc 681 Cor Tel Fax	ck Eng 7 Leo pus C ephon c: 361	jineerii pard S hristi, e: 36 ⁻ -883-4	ng & T Street Texas 1-883 711	esting 7840 4555	g Lab. Ii 9	nc		CLIENT: Belaire Environmental, Inc. PROJECT: Port of Port Lavaca (SWG-2016-01066) LOCATION: Calhoun County, Texas NUMBER: G122209 DATE(S) DRILLED: 4/19/2022
	FIF		ΤΑ	-Α		ABC	RAT	OR		A		DRILLING METHOD(S):
						AT	TERB	ERG				Solid Stem Auger
BOL		JUMBER		FT D FT D FT S O FT	E CONTENT (%)	) LIMIT			SU.FT	SSIVE H FT)	). 200 SIEVE (%)	GROUNDWATER INFORMATION: Groundwater (GW) was not encountered during drilling.
SYM	<u>н</u>	PLE N	oLES	S/SNC	TUR	auid	LAST	LAST	DENS NDS/C	PRES NGTI S/SQ	S NO	
SOIL	DEPT	SAMF	SAMF	N: BLO D: TO D: TO	MOIS		_ ■ PL	_ Ē PI	POUN	STRE (TON)	MINU	DESCRIPTION OF STRATUM
	- 1 -	SH S-1		P= 4.5+	16	48	14	34			85	LEAN CLAY WITH SAND, brown, moist, very stiff. (CL)
	- 4 -	SH S-2		P= 4.5	24							FAT CLAY WITH SAND, dark brown, moist, very stiff.
LOG_OF_BORING G122209.GPJ ROCK_ETL.GDT 5/13/22	N - S1 Qc - S P - PC		DAF	RD PENE CONE PE PENETRO		TION ROM TER	TES IETE RESI	T RE R TE STA	SIST. ST IN NCE	ANCE		Boring was terminated at a depth of 5 feet. <b>REMARKS:</b> Drilling operations were performed by On Point Geophysical at GPS Coordinates N 28.670003° W 96.570207°

									LUC	JOF	BO	RING IR-2 SHEET 1 of 1
	Neo DE E		A WE	Roc 681 Cor Tel Fax	ck Eng 17 Leo rpus C ephon (: 361	gineeri pard S hristi, ie: 36 -883-4	ng & T Street Texas 1-883- 1711	esting 7840 4555	g Lab. I 9	nc		CLIENT: Belaire Environmental, Inc. PROJECT: Port of Port Lavaca (SWG-2016-01066) LOCATION: Calhoun County, Texas NUMBER: G122209 DATE(S) DBILLED: 4/10/2022
	FIE		)AT	ГА		LABC	ORAT	ORY	/ DAT	A		DRILLING METHOD(S):
						AT	TERB	ERG				Solid Stem Auger
OL		JMBER		D E E E	CONTENT (%)	LIMIT			U.FT	SIVE T)	200 SIEVE (%)	GROUNDWATER INFORMATION: Groundwater (GW) was not encountered during drilling.
SYMB	H (FT	LE N	LES	NS/F NS/SQ NS/SQ NS/SO	TURE	auid	ASTI	ASTI	DENSI DS/C	PRES NGTH S/SQ I	S NO.	
SOIL	DEPT	SAMF	SAMP	N: BLO DC: TO DC: TO	SIOW	LL	료 PL	료 PI	POUN	COMF STRE (TON:	MINU	DESCRIPTION OF STRATUM
	- 1 -	SH S-1		P= 2.5	29	64	17	47			91	FAT CLAY, dark gray, moist, stiff. (CH)
	- 4 -	SH S-2		P= 3.75	29							Same as above, dark brown, very stiff. Boring was terminated at a depth of 5 feet.
	N - S1 Qc - S P - PC			RD PENE CONE PE PENETRO	TRA ⁻ NET		TES 1ETE RES	T RE R TE ISTA		ANCE		REMARKS: Drilling operations were performed by On Point Geophysical at GPS Coordinates N 28.671742° W 96.570058°

												RING TR-3 SHEET 1 of 1		
	Rock Engineering & Testing Lab. Inc 6817 Leopard Street Corpus Christi, Texas 78409 Telephone: 361-883-4555 Fax: 361-883-4711										CLIENT: Belaire Environmental, Inc. PROJECT: Port of Port Lavaca (SWG-2016-01066) LOCATION: Calhoun County, Texas NUMBER: G122209			
				- ^						٨		DRILLING METHOD(S)		
				A			TERBI	ERG				Solid Stem Auger		
OL		JMBER		T FT SFT SFT	CONTENT (%)	LIMIT			L L L L L	eive T)	200 SIEVE (%)	GROUNDWATER INFORMATION: Groundwater (GW) was not encountered during drilling.		
YMB	H (FT)	N E	В	WS/F S/SQ S/SQ VS/SQ	URE		ASTIC	ASTIC	ENSI DS/CI	RESS IGTH /SQF	Ň			
OIL S	EPTH	AMPI	AMPL		IOIST		БГ/	i PL/	RY DI OUNE	OMPI TREN ONS	INUS	SURFACE ELEVATION: N/A		
ů V	ā	ŝ	\ <i>`</i> 0/	Źŭ⊢Ŏ	Σ		PL	PI		υ'nΕ	Σ	DESCRIPTION OF STRATUM		
	- 1 - - 2 -	SH S-1		P= 3.25	24	61	14	47			87	<u>FAT CLAY</u> , dark gray, moist, very stiff. (CH)		
	- 4 -	SH S-2		P= 4.5+	21							Same as above, dark brown.		
	N - ST Qc - S P - PC	TANE	DAF	RD PENE CONE PE PENETRO	TRA ⁻ INET		TES	T RE R TE ISTA		ANCE		REMARKS: Drilling operations were performed by On Point Geophysical at GPS Coordinates N 28.672393° W 96.567539°		

	LOG OF BC											RING IR-4 SHEET 1 of 1
	Rock Engineering & Testing Lab. Inc 6817 Leopard Street Corpus Christi, Texas 78409 Telephone: 361-883-4555 Fax: 361-883-4711										CLIENT: Belaire Environmental, Inc. PROJECT: Port of Port Lavaca (SWG-2016-01066) LOCATION: Calhoun County, Texas NUMBER: G122209	
									/ ח א ד	· ^	DRILLING METHOD(S)	
								ERG			<u> </u>	Solid Stem Auger
SYMBOL	Н (FT)	PLE NUMBER	LES	DWS/FT VS/SQ FT VS/SQ FT DNS/SQ FT	TURE CONTENT (%	QUID LIMIT	-ASTIC LIMIT	ASTICITY INDEX	DENSITY IDS/CU.FT	PRESSIVE NGTH S/SQ FT)	S NO. 200 SIEVE (%	GROUNDWATER INFORMATION: Groundwater (GW) was not encountered during drilling.
SOIL	DEPT	SAMF	SAMF	2: TOI	MOIS		_ Ē PI	_ <u>⊼</u> PI		STRE TON:	MINU	DESCRIPTION OF STRATUM
	- 1 -	SH S-1		P= 2.5	18	44	13	31			83	LEAN CLAY WITH SAND, dark gray, moist, stiff.
	- 4 -	SH S-2		P= 3.75	13							Same as above, brown, very stiff.
	N - ST Qc - S P - PC		DA	RD PENE CONE PE PENETRO	TRA	TION RON TER	TES ÆTE RES	T RE R TE ISTA	ESIST EST IN NCE	ANCE		REMARKS: Drilling operations were performed by On Point Geophysical at GPS Coordinates N 28.671827° W 96.565817°

									LOG	j OF	BO	RING IP-1 SHEET 1 of 1	
	Rock Engineering & Testing Lab. Inc 6817 Leopard Street Corpus Christi, Texas 78409 Telephone: 361-883-4555 Fax: 361-883-4711											CLIENT:       Belaire Environmental, Inc.         PROJECT:       Port of Port Lavaca (SWG-2016-01066)         LOCATION:       Calhoun County, Texas         NUMBER:       G122209	
	FIF			-Δ		ARC		ORY		Δ		DATE(S) DRILLED: 4/18/2022 DRILLING METHOD(S):	
							TERB	ERG				Grab Sample	
٥٢		JMBER		F FT D FT	CONTENT (%)	IMIT			ZI LI	T) T	200 SIEVE (%)	GROUNDWATER INFORMATION: Groundwater (GW) was not encountered during drilling.	
SYMB(	н (FT)	LE NL	LES	WS/F IS/SQ IS/SQ	rure		ASTIC	ASTIC	DS/CL	RESS VGTH \$/SQ F	NO.		
SOIL S	DEPTI	SAMP	SAMP	N: BLC	NOIS	Ĕ II	ੂ ਸ	ੂ ਸੂ		STREI TONS	MINUS	SURFACE ELEVATION: N/A DESCRIPTION OF STRATUM	
	- 1 - - 2 - - 3 - - 5 -	GRAI S-1	 	Qc= 2	23	58	14	44			90	FAT CLAY, brown, moist, soft. (CH)	
	- 7 · - 8 · - 9 ·	- GRAI S-2	B	<del>Qc= 1</del>	51	71	16	55			90	FAT CLAY, gray, moist, soft. (CH) Boring was terminated at a depth of 10 feet.	
	N - S1 Qc - S P - PC		DAF IC T	RD PENE CONE PE PENETRO	TRA ⁻ NET DME	FION ROM TER	TES 1ETE RESI	T RE R TE ISTA	SIST, ST IN NCE	ANCE IDEX		REMARKS: Drilling operations were performed by Port Authority at GPS Coordinates N 28.64007° W 96.55535°	

										RING IP-2 SHEET 1 of 1			
	Rock Engineering & Testing Lab. Inc 6817 Leopard Street Corpus Christi, Texas 78409 Telephone: 361-883-4555 Fax: 361-883-4711											CLIENT: Belaire Environmental, Inc. PROJECT: Port of Port Lavaca (SWG-2016-01066) LOCATION: Calhoun County, Texas NUMBER: G122209 DATE(S) DRILLED: 4/18/2022	
	FIELD DATA LABORATORY DATA										DRILLING METHOD(S):		
						AT	TERBI	ERG				Grab Sample	
30L	-	IUMBER		er 2 Fr 2 Fr	E CONTENT (%)	LIMIT			ат Хи.FT	SIVE H FT)	. 200 SIEVE (%)	GROUNDWATER INFORMATION: Groundwater (GW) was not encountered during drilling.	
SYME	H (FI	LE N	LES	I/S/S/S/S/S/S/S/S/S/S/S/S/S/S/S/S/S/S/S	TURE	aub	-AST	-AST	DENS	PRES NGTH S/SQ	S NO		
SOIL	DEPT	SAMF	SAMF		MOIS	 LL	료 PL	PI	POUN	STRE TON:	MINU	DESCRIPTION OF STRATUM	
	- 1 · - 2 · - 3 · - 4 · - 5 ·	-  	 3,∞,		59	111	30	81			99	FAT CLAY, gray, moist, soft. (CH)	
		GRAI S-2	3 ₁₀₇		39	55	17	38			81	Same as above, gray and brown. (CH)	
	- 8 -	-		<del>Qc= 1</del>								Boring was terminated at a depth of 8 feet	
DRING G122209.GPJ ROCK_ETL.GDT 5/13/22							TEO					REMARKS:	
LOGOFBC	Qc - S Qc - S P - PC	STAT DCKE		CONE PERE PENETRO	NET OME	ROM	IETE RESI	R TE	SIST ST IN NCE	IDEX		Drilling operations were performed by Port Authority at GPS Coordinates N 28.63936° W 96.55729°	



Engineering & Testing Laboratory, Inc.

Rock Engineering & Testing Laboratory 6817 Leopard Street Corpus Christi, TX 78409-1703 Telephone: 361-883-4555 Fax: 361-883-4711

			KEY TO	SOIL CLASSIFICATION AND S	SYMBOLS			
	UNIFIE	SOIL CLASS	IFICATION SYST	ГЕМ	TERMS	CHARACTEF	RIZING SOIL	
MAJOR D	IVISIONS	SYMBOL		NAME		STRUCTUR	RE	
		GW	Well Graded G little or no fines	ravels or Gravel-Sand mixtures,	SLICKENSIDED weakness that	- having inclin are slick and	ed planes of glossy in	
	GRAVEL AND	GP	Poorly Graded little or no fines	Gravels or Gravel-Sand mixture	s, FISSURED - cor	FISSURED - containing shrinkage cracks, frequently filled with fine sand or silt; usually more or less vertical		
	GRAVELLY SOILS	GM	Silty Gravels, G	Gravel-Sand-Silt mixtures				
COARSE		GC	Clayey Gravels	, Gravel-Sand-Clay Mixtures	of varying colo sand or silt at t	r and texture, i the bottom to c	usually grading from clay at the top	
SOILS		SW	Well Graded Sa fines	ands or Gravelly Sands, little or	no CRUMBLY - coh blocks or crum	esive soils whi bs on drying	ich break into small	
	SAND	SP	Poorly Graded no fines	Sands or Gravelly Sands, little o	or CALCAREOUS of calcium carl	<ul> <li>containing ap conate, genera</li> </ul>	preciable quantities ally nodular	
	SANDY SOILS	SM	Silty Sands, Sa	nd-Silt Mixtures	WELL GRADED and substantia particle sizes	- having wide I amounts of a	range in grain sizes Il intermediate	
		SC	Clayey Sands,	Sand-Clay mixtures	POORLY GRAD size uniformly	ED - predomir graded) or hav	nantly of one grain ving a range of sizes	
		ML	Inorganic Silts a Silty or Clayey	and very fine Sands, Rock Flou fine Sands or Clayey Silts	with some inte ; graded)	with some intermediate size missing (gap or skip graded)		
	SILTS AND CLAYS	CL	Inorganic Clays Gravelly Clays, Clays	s of low to medium plasticity, Sandy Clays, Silty Clays, Lean	SYMI	30LS FOR TE	ST DATA	
FINE		OL	Organic Silts ar plasticity	nd Organic Silt-Clays of low	<u> </u>	Groundwater Le (Initial Reading)	evel	
SOILS		мн	Inorganic Silts, Sandy or Silty s	Micaceous or Diatomaceous fir soils, Elastic Silts	ie	(Final Reading)	evel	
	SILTS AND CLAYS	СН	Inorganic Clays	s of high plasticity, Fat Clays	■	SPT Samples	mpie	
		ОН	Organic Clays o Organic Silts	of medium to high plasticity,	<b>D</b>	Auger Sample		
HIGHLY ORGANIC SOILS PT $\frac{\sqrt{1}}{2} \frac{\sqrt{1}}{\sqrt{1}}$ Peat and othe		Peat and other	Highly Organic soils	0 -	Rock Core			
			TERMS	DESCRIBING CONSISTENCY	OF SOIL			
	COARSE C	BRAINED SOIL	S		FINE GRAINED SO	ILS		
DESCRIPTIVE TERM		NO. I STAN	BLOWS/FT. DARD PEN. TEST	DESCRIPTIVE TERM	NO. BLOWS/FT. STANDARD PEN TEST	. ( T(	UNCONFINED COMPRESSION DNS PER SQ. FT.	
Very Loose Loose Medium Dense Very Dense			0 - 4 4 - 10 10 - 30 30 - 50 over 50	Very Soft Soft Firm Stiff Very Stiff Hard	< 2 2 - 4 4 - 8 8 - 15 15 - 30 over 30	< 2         < 0.25           2 - 4         0.25 - 0.50           4 - 8         0.50 - 1.00           8 - 15         1.00 - 2.00           15 - 30         2.00 - 4.00           over 30         over 4.00		
				Field Classification for "Cons	sistency" is determined	with a 0.25" dia	ameter penetrometer	

# SLOPE STABILITY ANALYSIS RESULTS



- GEOTECHNICAL ENGINEERING
- CONSTRUCTION MATERIALS
   ENGINEERING & TESTING
- SOILS ASPHALT CONCRETE

### Slope

## SLOPE STABILITY ANALYSYS SHORT-TERM CONDITIONS



May 31, 2022 Attn: Ms. Laura Fox RETL Job Number G122209 BENEFICIAL USE MITIGATION (SWG-2016-01066) Port of Port Lavaca Calhoun County, Texas

#### **ROCK ENGINEERING & TESTING LABORATORY, INC.**

#### Corpus Christi

Office: 361.883.4555 Fax: 361.883.4711 6817 Leopard St. Corpus Christi, TX 78409

#### San Antonio

Office: 210.495.8000 Fax: 210.495.8015 10856 Vandale San Antonio, TX 78216

#### **Round Rock**

Office: 512.284.8022 Fax: 512.284.7764 7 Roundville Ln. Round Rock, TX 78664



- GEOTECHNICAL ENGINEERING
- CONSTRUCTION MATERIALS ENGINEERING & TESTING
- SOILS ASPHALT CONCRETE



Name: Berm	Unit Weight: 100 pcf	Cohesion': 30 psf	Phi': 25 °
Name: Clay 1	Unit Weight: 115 pcf	Cohesion': 40 psf	Phi': 28 °
Name: Clay 2	Unit Weight: 120 pcf	Cohesion': 110 psf	Phi': 29 °
Name: Clay 3	Unit Weight: 120 pcf	Cohesion': 240 psf	Phi': 28 °
Name: Clay 4	Unit Weight: 120 pcf	Cohesion': 290 psf	Phi': 29 °
Name: Clay 5	Unit Weight: 120 pcf	Cohesion': 200 psf	Phi': 28 °
Name: Clay 6	Unit Weight: 120 pcf	Cohesion': 150 psf	Phi': 27 °
Name: Clay 7	Unit Weight: 120 pcf	Cohesion': 300 psf	Phi': 26 °

May 31, 2022 Attn: Ms. Laura Fox RETL Job Number G122209 **BENEFICIAL USE MITIGATION (SWG-2016-01066)** 

Port of Port Lavaca Calhoun County, Texas

#### **ROCK ENGINEERING & TESTING LABORATORY, INC.**

#### Corpus Christi

Office: 361.883.4555 Fax: 361.883.4711 6817 Leopard St. Corpus Christi, TX 78409

#### San Antonio

Office: 210.495.8000 Fax: 210.495.8015 10856 Vandale San Antonio, TX 78216 **Round Rock** 

Office: 512.284.8022 Fax: 512.284.7764 7 Roundville Ln. Round Rock, TX 78664

# COMPATION TEST RESULTS



Rock Engineering - Corpus Christi 6817 Leopard St Corpus Christi, TX 78409 Ph: 361-883-4555 TXPE Firm Registration No. 2101

Client: Belaire Environmental, Inc. PO Box 741 Rockport Texas 78381 Project: Port of Port Lavaca (SWG-2016-01066) Calhoun County, Texas G122209

CC:

Sample Detai	ls			
Sample ID:	CC22-W02360-S01	Date Sample	ed:	
Sampled By:		Sampling Me	athod: Composite Grab Sample	
Material:	Reddish Brown & Light Gray Clay			
Sample Location:	TP-1 Dredge			
Tested By:	Christopher Rios	Date Tested:	5/7/2022	
99.0 98.0 97.0 96.0 97.0 96.0 97.0 96.0 97.0 96.0 97.0 96.0 97.0 96.0 97.0 96.0 97.0 96.0 97.0 96.0 97.0 97.0 97.0 97.0 97.0 97.0 97.0 97	ht - Water Content Relationship 0% Air Voids		Test Results ASTM D 698 Maximum Dry Unit Weight (Ibf/ft ³ ): Optimum Water Content (%): Method: Preparation Method: Specific Gravity (Fines): Retained Sieve No 4 (4.75mm) (%): Passing Sieve No 4 (4.75mm) (%): Tested By: Date Tested:	98.9 22.4 A 2.65 0 100 Christopher Rios 5/7/2022
90.0		$\langle \rangle$		
88.0	.0 20.0 21.0 22.0 23.0 24.0 25.0 26.0 27.0 26.0 29.0 30.0	31.0 32.0		
	Water Content (%)			

Comments

Form No: 110031, Report No: PTR:CC22-W02360-S01



**DMSA Borrow Area Overview: Source Material for Mitigation Site Construction CPA-Bean Tract Mitigation** Point Comfort, Calhoun County, Texas

Notes:

-Survey was conducted 3-31-2022. Basemap Source: ESRI ArcGIS Imagery... For planning purposes only, not for construction. Prepared by Belaire Environmental, Inc. 4-1-2022 (AP)



Depth of Red Clay Approximately 4 25 ft

Depth of Red Clay Approximately 4.27 ft

Depth of Red Clay Approximately 5 55 ft

**New Dredged** Material **Placement Footprint** 

Depth of Red Clay

Approximately 3,94 ft

Note:

Topo sample points recorded were within +/- 1 foot of the previous topo points recorded. One point was significantly higher, however, that sample point was outside of the material placement boundary.

Depth of Red Clay Approximately 5 22 ft

> Perimeter of **Borrow Area for** Mitigation Site Construction

Depth of Red Clay Approximately 5.39 ft Equip Access for **Current Dredging** 

_D#1

VEGETATION

PHOTOS CPA Mitigation Borrow Area BEI Field Investigation 3-30-2022

> Vegetated area-Existing Dredged Material (targeted for Borrow Area)

Red clay road-Newly Dredged Material







# **SCOPE OF WORK:**

# SURVEY OF BELAIRE ENVIRONMENTAL BEAN TRACT MITIGATION SITE, LAVACA BAY, TEXAS





NOTES:         1. SURVEY IS BASED ON NAD '83 (2011 EPOCH), TEXAS STATE PLANE COORDINATE SYSTEM, SOUTH CENTRAL ZONE, US FEET. TMI CONTROL POINT: N; 13,435,506.24 E; 2,747,683.36 Z: 18.76'         2. SURVEY WAS CONDUCTED ON APRIL 7, 2022 AND REPRESENTS THE CONDITIONS AT THAT TIME.         3. SURVEY WAS CONDUCTED ON 50 FOOT TRANSECTS         4. THIS SURVEY WAS CONDUCTED USING A GEOMETRICS G-882 MAGNETOMETER, A 200KHz TRANSDUCER, AND RTK-GNSS.		
NOTES: 1. SURVEY IS BASED ON NAD '83 (2011 EPOCH), TEXAS STATE PLANE COORDINATE SYSTEM, SOUTH CENTRAL ZONE, US FEET. TMI CONTROL POINT: N; 13,435,506.24 E; 2,747,683.36 Z: 18.76' 2. SURVEY WAS CONDUCTED ON APRIL 7, 2022 AND REPRESENTS THE CONDITIONS AT THAT TIME. 3. SURVEY WAS CONDUCTED ON 50 FOOT TRANSECTS 4. THIS SURVEY WAS CONDUCTED USING A GEOMETRICS G-882 MAGNETOMETER, A 200KHz TRANSDUCER, AND RTK-GNSS.	 NOTES	_
	<ul> <li>NOTES:</li> <li>1. SURVEY IS BASED ON NAD '83 (2011 EPOCH), TEXAS STATE PLANE COORDINATE SYSTEM, SOUTH CENTRAL ZONE, US FEET. TMI CONTROL POINT: N; 13,435,506.24 E; 2,747,683.36 Z: 18.76'</li> <li>2. SURVEY WAS CONDUCTED ON APRIL 7, 2022 AND REPRESENTS THE CONDITIONS AT THAT TIME.</li> <li>3. SURVEY WAS CONDUCTED ON 50 FOOT TRANSECTS</li> <li>4. THIS SURVEY WAS CONDUCTED USING A GEOMETRICS G-882 MAGNETOMETER, A 200KHz TRANSDUCER, AND RTK-GNSS.</li> </ul>	

# SURVEY OF BELAIRE ENVIRONMENTAL BEAN TRACT MITIGATION SITE LAVACA BAY, TEXAS

**OVERALL PROJECT LOCATION** (NOT TO SCALE)



PRE-CONSTRUCTION BATHYMETRIC SURVEY OF:

BEAN TRACT MITIGATION SITE

LOCATED IN LAVACA BAY, TEXAS

DATE: 4/14/22	DRAWN BY: CA
PROJECT No: 2589	SHEET: 1 OF 8



-UNITED BRINE PIPELINE

<u>1</u>7

LAVACA BAY





BEAN TRACT MITIGATION SITE

LOCATED	IN	LAVACA	BAY,	TEXAS
ATE 4/44/	~~~~			

DATE: 4/14/2022	DRAWN BY: CA
PROJECT No: 2589	SHEET: 2 OF 8


1000	100	1000	ACCURATE AND A
MAC	<i>FNETOM</i>	ETER TA	$4RGETS = \bigcirc$
POINT #	LATITUDE	LONGITUDE	DESCRIPTION
10	28.670116	96.571025	MONOPOLE 40
11	28.670866	96.570808	DIPOLE 140
12	28.671111	96.570736	MONOPOLE 150
13	28.671488	96.570662	MONOPOLE 40
14	28.671078	96.570896	MONOPOLE 800
15	28.672028	96.570704	DIPOLE 1500
16	28.671371	96.570994	DIPOLE 65
17	28.671658	96.570924	MONOPOLE 15
18	28.671777	96.570870	MONOPOLE 15
19	28.669890	96.571321	DIPOLE 40
20	28,669913	96.571322	
20	28 669804	96 571538	
21	28.669845	96,571532	
22	28.671613	96 571065	MONOPOLE 30
23	28 672163	96 570936	MONOPOLE 45
27	28.671639	96 571245	
25	28.071033	96 571189	
20	20.072013	96.571366	
2/	20.071707	90.571500	
28	28.009013	96.572058	
29	28.070254	96.572035	
30	28.670311	96.572015	MONOPOLE 50
31	28.672432	96.571525	MONOPOLE 60
32	28.670621	96.572158	DIPOLE 750
33	28.6/189/	96.571838	DIPOLE 140
34	28.6/2002	96.571803	MONOPOLE 50
35	28.672024	96.571929	MONOPOLE 25
36	28.6/1011	96.5/21//	DIPOLE 10
37	28.669476	96.572755	DIPOLE 30
38	28.670815	96.572555	DIPOLE 200
39	28.672585	96.572078	MONOPOLE 50
40	28.671235	96.572661	MONOPOLE 90
41	28.671964	96.572415	MONOPOLE 40
42	28.672203	96.572342	DIPOLE 30
43	28.672181	96.572430	MONOPOLE 200
44	28.672377	96.572403	MONOPOLE 150
45	28.669607	96.573159	MONOPOLE 25
46	28.669635	96.573256	MONOPOLE 200
47	28.669660	96.573507	MONOPOLE 80
48	28.670246	96.573330	DIPOLE 40
49	28.672050	96.572946	DIPOLE 120
50	28.670609	96.573398	DIPOLE 60
51	28.671935	96.573066	DIPOLE 100
52	28.672075	96.573023	DIPOLE 200
53	28.669536	96.573837	MONOPOLE 75
54	28.672105	96.573264	MONOPOLE 4000
	28.672180	96.573217	DIPOLE 3500
55			
55 56	28.672168	96.573590	MONOPOLE 6000
55 56 57	28.672168 28.672346	96.573590 96.573574	MONOPOLE 6000 MONOPOLE 1000



PRE-CONSTRUCTION BATH	YMETRIC SURVEY OF:
BEAN TRACT MIT.	IGATION SITE
LOCATED IN LAVAC	A BAY, TEXAS
DATE: 4/14/2022	DRAWN BY: CA
PROJECT No: 2589	SHEET: 3 OF 8

X: 2746383.88			0+00.TIN			Length: 1200.00		Azimuth: 1	01.08
Y: 13435421.26	0.00	100.00	200.00	300.00	400.00	500.00	600.00	700.00	800.
30.00		1	1			1	1	1	1
25.00									
20.00									
15.00									
						0+00			
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NOTES: 1. SURVEY IS BASED ON NAD '83 (2011 EPOCH), TEXAS STATE PLANE COORDINATE SYSTEM, SOUTH CENTRAL ZONE, US FEET. TMI CONTROL POINT: N: 13,435,506.24 E: 2,747,683.36 Z: 18.76' 2. ELEVATIONS ARE SHOWN IN NAVD'88. 3. SURVEY WAS CONDUCTED ON APRIL 7, 2022 AND REPRESENTS THE CONDITIONS AT THAT TIME. 4. SURVEY WAS CONDUCTED ON 50 FOOT TRANSECTS 5. THIS SURVEY WAS CONDUCTED USING A 200KHz TRANSDUCER AND RTK-GNSS.	



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TMI SOLUTIONS LLC
361.688.6785 WWW.TMISOLUTIONSLLC.COM GEORGE WEST, TEXAS 78022

PRE-CONSTRUCTION BATHYMETRIC SURVEY OF:

BEAN TRACT MITIGATION SITE

LOCATED IN LAVACA BAY, TEXAS

DATE: 4/14/2022	DRAWN BY: CA
PROJECT No: 2589	SHEET: 4 OF 8

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PRE-CONSTRUCTION BATHYMETRIC SURVEY OF:

BEAN TRACT MITIGATION SITE

LOCATED IN LAVACA BAY, TEXAS

DATE: 4/14/2022	DRAWN BY: CA
PROJECT No: 2589	SHEET: 5 OF 8

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LOCATED IN LAVACA BAY, TEXAS

DATE: 4/14/2022	DRAWN BY: CA
PROJECT No: 2589	SHEET: 6 OF 8



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04-08-22 SURV	EY								

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 4. SURVEY WAS CONDUCTED ON 50 FOOT TRANSECTS 5. THIS SURVEY WAS CONDUCTED USING A 200KHz TRANSDUCER AND RTK-GNSS. 	





BEAN TRACT MIT	TIGATION SITE
LOCATED IN LAVAG	CA BAY, TEXAS
DATE: 4/14/2022	DRAWN BY: CA
PROJECT No: 2589	SHEET: 7 OF 8

PRE-CONSTRUCTION BATHYMETRIC SURVEY OF:

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TMI SOLUTIONS LLC
361.688.6785 WWW.TMISOLUTIONSLLC.COM GEORGE WEST, TEXAS 78022

PRE-CONSTRUCTION BATHYMETRIC SURVEY OF:

BEAN TRACT MITIGATION SITE

LOCATED IN LAVACA BAY, TEXAS

ATE: 4/14/2022 DRAWN BY: CA

DATE: 4/14/2022	DRAWN BY: CA
PROJECT No: 2589	SHEET: 8 OF 8

SCOPE OF WORK: DEPART OF THE ARMY PERMIT SWG-2016-01066

DEPARTMENT OF THE ARMY PERMIT

Permittee Calhoun Port Authority

Permit No. SWG-2016-01066

Issuing Office Galveston District

NOTE: The term "you" and its derivatives, as used in this permit, means the permittee or any future transferee. The term "this office" refers to the appropriate district or division office of the Corps of Engineers having jurisdiction over the permitted activity or the appropriate official of that office acting under the authority of the commanding officer.

You are authorized to perform work in accordance with the terms and conditions specified below.

Project Description: To dredge and discharge fill material into tidal waters of the United States (US) and adjacent wetlands associated with the construction of a new marine terminal. The terminal will consist of 3 deep-water liquid product docks, 6 shallow-draft liquid product barge docks, and related appurtenant shore facilities. The proposed work includes the following: 1) installation of approximately 3,430 linear feet of steel sheet pile bulkhead for stabilization and barge mooring; 2) mechanical dredging of approximately 2.615 million cubic yards (mcy) of material from the project site and the adjacent Matagorda Ship Channel to -47 feet mean lower low water (MLLW), plus an allowable 2-foot advanced maintenance dredge and 2-foot over-dredge for the deep-water docks, and -14 feet MLLW, plus an allowable 2-foot advanced maintenance dredge and 2-foot over-dredge for the barge docks; 3) construction of an approximately 61-acre (940-foot-wide by 2,800-foot-long) dredge material stockpile area (DMSA) for future Port expansion; 4) relocation and repair on the southern levee of the applicant's existing Dredge Material Placement Area (DMPA) 1, located approximately 2,700 feet west-northwest of the proposed new terminal, across the Matagorda Ship Channel. Project impacts include the following: dredging of approximately 40.75 acres of open waters of the US and 0.83 acre of adjacent estuarine emergent wetlands, and the permanent discharge of fill material within approximately 11.95 acres of adjacent estuarine emergent wetlands and approximately 21 acres of open waters of the US.

The project will be conducted in accordance with the attached plans, in 33 sheets.

Project Location: The project site is located in Lavaca and Matagorda Bays, and adjacent wetlands, at the Port of Port Lavaca-Point Comfort approximately 2.4 miles south-southwest of the intersection of the Texas State Highway 35 and Farm-to-Market (FM) Road 1593, in Point Comfort, Calhoun County, Texas.

Permit Conditions:

General Conditions:

1. The time limit for completing the work authorized ends on <u>31 December 2025</u>. If you find that you need more time to complete the authorized activity, submit your request for a time extension to this office for consideration at least one month before the above date is reached.

2. You must maintain the activity authorized by this permit in good condition and in conformance with the terms and conditions of this permit. You are not relieved of this requirement if you abandon the permitted activity, although you may make a good faith transfer to a third party in compliance with General Condition 4 below. Should you wish to cease to maintain the authorized activity or should you desire to abandon it without a good faith transfer, you must obtain a modification of this permit from this office, which may require restoration of the area.

3. If you discover any previously unknown historic or archeological remains while accomplishing the activity authorized by this permit, you must immediately notify this office of what you have found. We will initiate the Federal and state coordination required to determine if the remains warrant a recovery effort or if the site is eligible for listing in the National Register of Historic Places.

4. If you sell the property associated with this permit, you must obtain the signature of the new owner in the space provided and forward a copy of the permit to this office to validate the transfer of this authorization.

5. If a conditioned water quality certification has been issued for your project, you must comply with the conditions specified in the certification as special conditions to this permit. For your convenience, a copy of the certification is attached if it contains such conditions.

6. You must allow representatives from this office to inspect the authorized activity at any time deemed necessary to ensure that it is being or has been accomplished in accordance with the terms and conditions of your permit.

Special Conditions:

1. The permittee understands and agrees that, if future operations by the United States require the removal, relocation, or other alteration, of the structure or work herein authorized, or if, in the opinion of the Secretary of the Army or his authorized representative, said structure or work shall cause unreasonable obstruction to the free navigation of the navigable waters, the permittee will be required, upon due notice from the Corps of Engineers, to remove, relocate, or alter the structural work or obstructions caused thereby, without expense to the United States. No claim shall be made against the United States on account of any such removal or alteration.

2. When structures or work authorized by this permit are determined by the District Engineer to have become abandoned, obstructive to navigation or cease to be used for the purpose for which they were permitted, such structures or other work must be removed, the area cleared of all obstructions, and written notice given to the Corps of Engineers, Galveston District, Regulatory Division, within 30 days of completion.

3. The permittee must install and maintain, at the permittee's expense, any safety lights, signs and signals required by US Coast Guard, through regulations or otherwise, on the permittee's fixed structures. To receive a US Coast Guard Private Aids to Navigation marking determination, at no later than 30 days prior to installation of any fixed structures in navigable waters and/or prior to installation of any floating private aids to navigation, you are required to contact the Eighth Coast Guard District (dpw), 500 Poydras St., Suite 1230, New Orleans, LA 70130, (504) 671-2328 or via email to: D8oanPATON@uscg.mil. For general information related to Private Aids to Navigation please visit the Eighth Coast Guard District-8/District-8/District-Divisions/Waterways/PATON/

4. All construction of mitigation must be started within 12 -18 months after start of construction within jurisdictional areas. The permittee will notify the Corps of Engineers, Galveston District (CESWG), Chief, Compliance Branch, Regulatory Division in writing when the work begins in jurisdictional areas. Performance standards, reporting, monitoring, and maintenance will proceed according to the compensatory mitigation plan.

5. Should mitigation be determined to be unsuccessful by CESWG personnel at the end of the monitoring period, the permittee will be required to take necessary correction measures, as approved by the CESWG. Once the corrective measures are completed, the permittee will notify the CESWG, Chief, Compliance Branch, Regulatory Division, in writing, and a determination will be made regarding success of the mitigation.

Further Information:

- 1. Congressional Authorities: You have been authorized to undertake the activity described above pursuant to:
- (X) Section 10 of the Rivers and Harbors Act of 1899 (33 U.S.C. 403).
- (X) Section 404 of the Clean Water Act (33 U.S.C. 1344).
- () Section 103 of the Marine Protection, Research and Sanctuaries Act of 1972 (33 U.S.C. 1413).
- 2. Limits of this authorization.
 - a. This permit does not obviate the need to obtain other Federal, state, or local authorizations required by law.
 - b. This permit does not grant any property rights or exclusive privileges.
 - c. This permit does not authorize any injury to the property or rights of others.
 - d. This permit does not authorize interference with any existing or proposed Federal project.

3. Limits of Federal Liability. In issuing this permit, the Federal Government does not assume any liability for the following:

a. Damages to the permitted project or uses thereof as a result of other permitted or unpermitted activities or from natural causes.

b. Damages to the permitted project or uses thereof as a result of current or future activities undertaken by or on behalf of the United States in the public interest.

c. Damages to persons, property, or to other permitted or unpermitted activities or structures caused by the activity authorized by this permit.

d. Design or construction deficiencies associated with the permitted work.

e. Damage claims associated with any future modification, suspension, or revocation of this permit.

4. Reliance on Applicant's Data: The determination of this office that issuance of this permit is not contrary to the public interest was made in reliance on the information you provided.

5. Reevaluation of Permit Decision. This office may reevaluate its decision on this permit at any time the circumstances warrant. Circumstances that could require a reevaluation include, but are not limited to, the following:

- a. You fail to comply with the terms and conditions of this permit.
- b. The information provided by you in support of your permit application proves to have been false, incomplete, or inaccurate (See 4 above).
- c. Significant new information surfaces which this office did not consider in reaching the original public interest decision.

Such a reevaluation may result in a determination that it is appropriate to use the suspension, modification, and revocation procedures contained in 33 CFR 325.7 or enforcement procedures such as those contained in 33 CFR 326.4 and 326.5. The referenced enforcement procedures provide for the issuance of an administrative order requiring you to comply with the terms and conditions of your permit and for the initiation of legal action where appropriate. You will be required to pay for any corrective measures ordered by this office, and if you fail to comply with such directive, this office may in certain situations (such as those specified in 33 CFR 209.170) accomplish the corrective measures by contract or otherwise and bill you for the cost.

6. Extensions. General Condition 1 establishes a time limit for the completion of the activity authorized by this permit. Unless there are circumstances requiring either a prompt completion of the authorized activity or a reevaluation of the public interest decision, the Corps will normally give favorable consideration to a request for an extension of this time limit.

Your signature below, as permittee, indicates that you accept and agree to comply with the terms and conditions of this permit.

(PERMITTEE) CALHOUN PORT AUTHORITY

<u>9 - 9 - 20</u> (DATE)

This permit becomes effective when the Federal official, designated to act for the Secretary of the Army, has signed below.

(DISTRICT ENGINEER) KRISTI N. MCMILLAN LEADER, CENTRAL EVALUATION UNIT FOR COLONEL TIMOTHY R. VAIL (DATE)

When the structures or work authorized by this permit are still in existence at the time the property is transferred, the terms and conditions of this permit will continue to be binding on the new owner(s) of the property. To validate the transfer of this permit and the associated liabilities associated with compliance with its terms and conditions, have the transferee sign and date below.

(TRANSFEREE – Typed/Printed Name)

(DATE)

(TRANSFEREE - Signature)

(Mailing Address)

































PERMITTED PLANS

MITIGATION PLAN AT BEAN TRACT PERMIT NO. SWG-2016-01066 CALHOUN PORT AUTHORITY LAVACA BAY, CALHOUN COUNTY, TEXAS

Prepared for: Calhoun Port Authority PO Box 397 Point Comfort, Texas 77978

Prepared by: Belaire Environmental, Inc. P.O. Box 741 Rockport, TX 78381

August 4, 2020



Mitigation Plan SWG-2006-010166 Lavaca Bay near Point Comfort, Calhoun County, Texas August 4, 2020

PERMITTED PLANS

The April 10, 2008 USACE/EPA Final Mitigation Rule (2008 Mitigation Rule) outlines 12 Fundamental Components to be uniformly addressed in all compensatory mitigation plans (33 CFR 332.4(c)(2) through (c)(14)) for the purposes of developing successful compensatory mitigation projects and facilitating effective compliance measures. According to the 2008 Mitigation Rule, "the level of detail of the mitigation plan should be commensurate with the scale and scope of the impacts." The information below outlines the 12 Fundamental Components of Calhoun Port Authority's (CPA) proposed compensatory mitigation plan.

I. Objective of the Compensatory Mitigation Plan

- A. Method of Compensation
 - The proposed mitigation plan involves the creation of an approximately 14-acre marsh system in Lavaca Bay. The mitigation site would consist of approximately 10 acres of high and low marsh, approximately 1 acre of circulation channels, and 3.0 acres of levee protection. Approximately 1,775 linear feet of articulated matting would be placed on the bayward side of the mitigation area in order to protect the site from wave energy.
 - 2. See Exhibit A for Plan and Cross-section drawings of the proposed mitigation site features. The proposed mitigation plan involves the beneficial use (BU) of approximately 60,000 to 80,000 cu yds of suitable (appropriate physical engineering and chemical properties) dredged material or use of other suitable clean fill material as approved by the USACE. The USACE permit will contain conditions requiring testing of material for use in mitigation site construction for both physical properties and for potential contaminants. CPA will test any material proposed to be used for mitigation site construction prior to conducting work. Testing will include both geotechnical testing for physical properties of the material, as well as contaminant testing in accordance with CPA's Sampling Analysis Plan (SAP) to ensure that suitable material is used for mitigation site construction. The SAP will be approved in advance by the USACE.

CPA has identified three alternatives for sourcing the material for mitigation site construction. Each alternative involves testing as described above, and only material that is determined to be suitable based upon testing results will be used. Alternative 1 involves utilizing material dredged from CPA's docks for the purpose of creating deep-water and shallow draft access to new docking areas to handle liquid petrochemicals. This dredged material would be pumped or mechanically placed into a confined leveed area at elevations suitable to create a network of intermixed low and high tidal marshes with circulation channels. The proposed dredge quantity involves approximately 2.615 million cubic yards, of which approximately 60,000 to 80,000 cubic yards is needed to construct the mitigation site. If Alternative 1 (utilizing project dredged material, after testing) does not identify suitable material, then CPA would pursue Alternative 2. Alternative 2 involves testing and using alternate material at an existing placement area within uplands at CPA facilities. In the event that material is found to be unsuitable then, for Alternative 3, CPA would identify a commercial source of clean fill material for constructing the mitigation site and test it as well prior to using it for mitigation site construction.

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The selected material, as approved by the USACE, would be placed into a confined leveed area at elevations suitable to create a network of intermixed low and high tidal marshes with circulation channels. Soil composition will largely dictate finished topographic features. An earthen levee will be constructed to contain the material. The portion of the levee exposed to wind and wave action would be armored with articulated concrete matting. This matting will also provide intertidal hard substrate for oyster and associated organisms to attach. The remainder of the levee will be lowered to elevations that support desirable wetland plant species. In the long-term, the breakwater will help protect the high and low marsh wetlands, as well as the currently eroding shoreline, from wave action and erosion.

Mitigation Habitat Creation (14 acres total)

- 1.3 acres of high marsh habitat (+2.0 to +3.0 ft NAVD 88)
- 8.7 acres of low marsh habitat (+0.5 ft to +1.65 ft NAVD 88)
- 1.0 acre of permanently inundated shallow water habitat (circulation channels). The circulation channels will be at elevations -2.0 to -3.0 feet NAVD 88 and would very rarely if ever be exposed.
- 3.0 acres of levee protection
- B. <u>Manner in which the resource functions of the mitigation will address the needs of the watershed or</u> region

The site's present-day condition consists of unvegetated bay bottom littered with assorted debris including abandoned vessels, pipe, and other materials. The proposed mitigation will provide a greater overall habitat value by enhancing the existing habitat functions and by creating new high marsh, low marsh, and shallow water edge habitat. The created habitat will be protected with armored levee to assure long-term resilience.

II. Site Selection

The applicant considered numerous options for the mitigation site including land owned by the TPWD, Powderhorn Ranch, privately owned land, and port-owned property. The TPWD site was initially selected, however after extensive coordination and evaluation TPWD decided they needed more extensive internal evaluations before they commit to such a mitigation effort at this location. The applicant ultimately selected the currently proposed submerged port-owned property because it offered a potential opportunity for beneficial use of dredged material, is a site with many past disturbances, is port-owned property, was a low value unvegetated disturbed bay bottom, was near the proposed port development project, was of suitable substrate and elevation for marsh creation and establishment, was protected from prevailing south-east winds, provided barge and road access and has a high likelihood of successful estuarine habitat development. The implementation of the project will establish low and high marsh areas with circulation channels as well as construction of an approximately 1,775-ft hard substrate breakwater. The chosen mitigation site will preserve these benefits.

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III. Site Protection Instrument

Within 6-months of the start of construction in jurisdictional areas, the permittee will consummate and record with the County Clerk of Calhoun County, restrictive covenants for the compensatory mitigation site.

IV. Baseline Information (Impact and Compensation Site)

A. Ecological Characteristics of the Impacted Site

As noted in the Public Notice, the impacted site is largely undeveloped land comprised of a previously authorized upland placement area, and an area that was historically open water. A large portion of the area for the proposed fill area has been heavily impacted by past, present, and projected dredge placement in the adjacent OBPAs. As a result, much of the area that was historically open water has been filled with sediment to an elevation close to or above the annual high tide line. Continued disposal at 18-month intervals is expected to convert the entire site to uplands within the next five years. The approximate 11.95 acres of estuarine wetlands proposed to be impacted by the project have only recently developed during the last growing season. As previously stated, the adjacent unconfined disposal will continue until the impact area is converted to upland.

B. Ecological Characteristics of the Compensation Site

Belaire Environmental, Inc. (BEI) conducted an oyster, wetland, and seagrass survey at the proposed B.U. site (November 25, 2019). The proposed mitigation site is a highly disturbed unvegetated bay bottom. Abandoned vessels, barges, pipe and various other debris litter the surrounding bay bottom. The adjacent shoreline experiences significant wind-wave erosion. The site is low value subtidal habitat. No oysters, wetlands, seagrass beds, or other sensitive resources were found in the proposed B.U. area. Some shoreline wetlands were observed nearby the proposed mitigation site. These existing wetlands will not be impacted by mitigation construction activities and would be protected from wind-wave erosion by the proposed permanent armored levee with articulated matting.

V. Determination of Credits

CPA has demonstrated significant efforts in avoiding and minimizing impacts to jurisdictional areas. At the area of impacts, Calhoun Port Authority (CPA) proposes to construct three deep-water liquid product docks, six shallow draft liquid product barge docks for the handling of liquid petrochemicals, and an approximate 3,430 linear feet of steel sheet pile bulkhead for barge mooring. The permit application was originally submitted to the USACE on February 2, 2018 with wetland impacts totaling 37.62 acres (1.31 acres due to construction of the bulkhead and 36.31 acres due to construction of the proposed new development area (NDA) for future facilities expansion). Subsequently, the footprint was reduced, and impacts to estuarine wetlands were revised to 33.4 acres. The proposed NDA in the permit application is located near the vicinity of U.S. Army Corps of Engineers (USACE) Open Bay Placement Areas (OBPA) No. 18 and 19. The USACE typically utilizes this unconfined placement area every 18 months and over the past eight years has discharged over three million cubic yards of material, not including the most recent dredge event. As a result of unconfined disposal of dredged material, the material is free to migrate.

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During a June 6, 2018 site visit with Kevin Mannie of the USACE, significant changes were observed at the proposed impact area due to migration of unconfined dredge material placement into DMPA 19. BEI surveyed the site on June 13, 2018, and survey results found an average of 0.98 ft of recent dredge material coverage above the stem/root mass interface covering approximately 21 acres within the proposed NDA. The estuarine wetland impacts associated with the project were revised to reflect the survey findings, and impacts were further reduced from 33.4 acres to 11.95 acres (a reduction of approximately 21 acres of estuarine wetland impacts) of estuarine wetlands and 2 sq ft of oyster shell.

At the recommendation of the USACE representative Kevin Mannie during the USACE June 6, 2018, site visit, BEI analyzed the wetland impact area at three different periods of time: 5 years prior (2013), current condition on June 6, 2018, and five years in the future (2023). For simplicity the project was broken down into two impact areas WAA#1 and WAA#2. The wetlands encompassed within WAA#1 are proposed to be impacted by the dredging and construction of a bulkhead. For simplicity, a consistent value was assigned for WAA#1 and used for each year. No discrepancy for the acreage or functional value of these wetlands was recognized. The wetlands encompassed within WAA#2 are the proposed wetland within the proposed dredge material stockpile area footprint. This footprint has been analyzed for impacts by conducting separate iHGM score sheets for each year (2013, 2018 and 2023) to calculate the average loss in function capacity units for the proposed DMSA area. A table of the potential functional capacity impacts at the project site follows.

Functional Capacity Units Lost (WAA 1 & WAA 2)									
2013 2018 2023 Average									
Biota (FCU)	-6.38	-15.74	-2.23	-8.12 FCU					
Botanical (FCU)	-3.12	-10.76	-1.18	-5.02 FCU					
Physical (FCU)	-3.29	-9.6	-0.88	-4.59 FCU					
Chemical (FCU)	-1.17	-3.46	-0.59	-1.74 FCU					

Potential Functional Capacity Impacts WAA 1 FCU biota loss (bl) + WAA 2 bl + WAA 3 bl + WAA 4 bl = net FCU loss

Potential Functional Capacity Gains WAA #3 (Bean Tract Mitigation Site)

(Functional Capacity Units (FCU); FCI x wetland acres per WAA)

11 Acres	Pre-project FCUs	Post project FCUs	Post – Pre
Biota	1.71 x 15.28 = 26.13 FCUs	2.05 x 26.28 = 53.87 FCUs	+27.74 GAIN
Botanical	1.0 x 15.28 = 15.28 FCUs	1.0 x 26.28 = 26.28 FCUs	+11.00 GAIN
Physical	0.54 x 15.28 = 8.25 FCUs	0.88 x 26.28 = 23.13 FCUs	+14.88 GAIN
Chemical	0.5 x 15.28 = 7.64 FCUs	0.5 x 26.28 = 13.14 FCUs	+5.50 GAIN

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SUMMARY OF NET GAINS

Biota: -8.12 (WAA 1&2) + 27.74 (WAA 3) = **19.62 Net FCU Gain**

Botanical: -5.02 (WAA 1&2) + 11.00 (WAA 3) = 5.98 Net FCU Gain

Physical: -4.59 (WAA 1&2) + 14.88 (WAA 3) = 10.29 Net FCU Gain

Chemical: -1.74 (WAA 1&2) + 5.50 (WAA 3) = 3.76 Net FCU Gain

The iHGM report submitted to the USACE as part of the October 12, 2018 permit application package, and summarized here, as compared to the iHGM report prepared for the proposed mitigation site (enclosed as Exhibit B) demonstrates that more than adequate compensation will be provided for the types and qualities of impacted aquatic resources. It is CPA's goal to utilize the existing intertidal unvegetated area to create a highly productive, diverse, and resilient estuarine habitat.

VI. Mitigation Work Plan

The mitigation plan allows for the creation of a confined (via levees and a hard structure breakwater or articulated matting) 14-acre mitigation site. The mitigation site's perimeter will be constructed as described below. After the confined site is constructed, material will be hauled by barges or trucks or hydraulically pumped from CPA's impact area, if that is the selected alternative for material sourcing, to the mitigation site. If hydraulic dredging is utilized, interior levees and weirs will be constructed to accommodate settling of TSS. An access route for the dredge pipe that is free of oysters, navigation hazards, and sensitive resources will be staked prior to placement of the dredge pipe. Alternately, the material would be mechanically transported and placed. Up to two temporary access roads with 70-ft top surface width may be constructed to provide equipment access if mechanical placement of material is used. Wetlands will be avoided for these access roads (Exhibit A).

The mitigation plan involves the creation of a 3.0-acre levee system, including:

- 1.8 acres of levee armored with articulated mats which will remain in place after completion of construction and dredging, and
- 1.2 acres of temporary levee.

Material excavated from within the site adjacent to the levees and/or hauled-in fill material will be used for levee construction. The entire levee, which will confine the placed dredged material, will be constructed to approximately +10.0 ft NAVD 88 during mitigation site construction in order to contain the material and allow for construction equipment to travel along the levee top for construction activities. After construction is complete and consolidation of dredged material has occurred, the 1.8 acres of armored levee (1,775 linear feet) will be lowered to +5.0 ft NAVD 88, and the 1.2 acres of temporary levee (1,190 linear ft) will be lowered to +2.0 to +3.0 ft NAVD 88 to allow for tidal influence.

The articulated matting to be used for the long-term protection of levee areas subjected to significant wind-wave erosion will likely facilitate oyster and barnacle attachment. BEI's past experience indicates this. Between 1990 & 2010, BEI planned, permitted, and assisted with installation of four similar mitigation projects at the ANWR. Monitoring studies found that all four

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established substantial oyster populations within the intertidal zone. In addition to protecting the mitigation site and plantings from wave action and erosion, it is likely that the mats will encourage oyster growth.

After mitigation site construction and levee contouring to finished grades, 10-acres (8.7 acres of low marsh and 1.3 acres of high marsh) would then be planted on 3-ft centers with appropriate estuarine species (e.g. smooth cordgrass (*Spartina alterniflora*) on side slopes and saltgrass (*Distichlus spicata*), seashore paspalum (*Paspalum vaginatum*), saltwort (*Batis maritima*), chicken claws (*Sarcocornia ambigua*), sea ox-eye daisy (*Borrichia frutescens*), etc.). This 1.3 acres will compensate for the loss of 1.3 acres of high marsh at the project site. Approx. 60,000 to 80,000 cu yds of suitable material from the harbor dredging project will be mechanically or hydraulically placed within the levees at elevations ranging from +0.5 to +1.65 ft NAVD 88 for planting smooth cordgrass on 3-ft centers. Nearby existing smooth cordgrass is established at these elevations. Prior to start of construction, additional nearby smooth cordgrass beds will be surveyed to refine these elevations for plans and specifications.

As stated on the Plan View drawing in Exhibit A, the mitigation site boundary is subject to minor changes based on further engineering and contractor evaluations. The location of planting benches and circulations may be slightly altered due to further evaluation of site conditions.

A. High Marsh Creation

Approximately 1.3 acres of existing unvegetated bay bottom located on the edges of the mitigation site will be mechanically or hydraulically filled with dredged material to elevations consistent with nearby reference high marsh areas. The precise locations of these created high marsh areas may be modified based on onsite conditions. High marsh species will be planted on 3-foot centers to vegetate the contoured areas. Signage will be installed in an effort to prohibit human activity within the high marsh creation areas. Mitigation construction will begin within 6-months of impacts to jurisdictional areas.

B. Low Marsh Creation

Approximately 8.7 acres of existing unvegetated bay bottom on at the mitigation site will be mechanically or hydraulically filled with dredged material to elevations consistent with nearby reference low marsh areas. Low marsh species, predominantly smooth cordgrass, will be planted to vegetate the contoured areas. A reference survey of adjacent low marsh areas will be conducted prior to construction in order to establish precise target elevations and coverage of natural marshes. Signage will be installed in an effort to prohibit human activity within the low marsh creation areas. Mitigation construction will begin within 6-months of impacts to jurisdictional areas.

C. <u>Circulation Channels</u>

Approximately 1 acre of unvegetated bay bottom will be left undisturbed or excavated to a depth of approximately -2.0 to -3.0 ft NAVD 88 for the creation of 20-ft wide circulation channels.

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D. <u>Planting</u>

The mitigation site will be planted with appropriate species once the dredged material has sufficiently consolidated. Following sediment conditioning of at least 60 days, the areas will be planted on 3-ft centers. A planting unit will consist of a small bareroot clump of each of the various salt marsh species. Each planting unit will be securely embedded in the planting surface. Low marsh areas will be planted with predominantly smooth cordgrass (*Spartina alterniflora*). Intermediate to high marsh areas will be planted with saltgrass (*Distichlis spicata*), saltwort (*Batis maritima*), glasswort (*Salicornia virginica*), sea ox-eye daisy (*Borrichia frutescens*), and associated species. A written report, including complete photographic coverage of the planting areas, shall be submitted to the USACE immediately prior to and following within 30 days of transplanting activities.

VII. Maintenance Plan

If substantial changes in the mitigation site are observed during monitoring events, the applicant will include these results in the monitoring report(s) and will set up a meeting with the U.S. Army Corps of Engineers (USACE) to determine an agreed upon path forward.

VIII. Performance Standards and Monitoring Requirements

CPA will be responsible for monitoring the site for a total of 5 years to track the success of created habitats through quantitative assessments of vegetative cover (as described below). A preconstruction aerial photograph of the site will be taken immediately prior to construction. Additionally, within 30 days after completion of construction activities an aerial photograph will be taken and a monitoring survey will be conducted to establish existing baseline as-built conditions.

High & Low Marsh Creation

Survival of transplanted species will be monitored 60 days after completion of planting. A report will be submitted to the USACE within 30 days of completion of this monitoring. The coverage of the target vegetation, in percent, will also be monitored within the high and low marsh mitigation areas and recorded in subsequent reports. Coverage monitoring reports will include photo documentation and will be submitted to the USACE at 6-months, 1-year, 2-years, 3-years, 4-years, and 5-years following the initial planting of the above habitat.

- A transplant survival survey will be conducted within 60 days following completion of the initial planting effort. If 50% survival of transplant material is not achieved, the USACE will be notified in writing and a 2nd planting effort will be made within the next 30 days or within the next seasonal high tide period (September 15 to November 15 or March 15 to June 15) using the original planting specifications.
- 2. If after one year from the initial planting effort (or subsequent planting efforts) the site does not have at least 35% aerial coverage of targeted vegetation, those areas that are not vegetated will be replanted within 60 days using the original planting specifications.
- 3. If at least 70% aerial coverage of the transplanted species for each respective plant community is not achieved within 3 years following initial planting, and additional re-

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planting will be performed within the next 30 days or within the next seasonal high tide period (September 15 to November 15 or March 15 to June 15) using the original planting specifications.

4. In addition to the initial 60-day survey report, progress reports will be submitted to USACE at 6 months, 1-year, 2-year, 3-year, 4-year, and 5-year intervals following the initial transplanting effort or subsequent replanting efforts. Photos of the mitigation site would be included. Any erosion or accretion, including circulation channels, will be documented during each monitoring effort.

If the established habitats mentioned above show significant change in the designated areas during any monitoring survey, a meeting will be held with CPA and USACE to determine if changes need to be made to the mitigation site.

IX. Long-term Management Plan

Long-term management of the site will be the responsibility of CPA. The entire mitigation site will be preserved in perpetuity via a conservation easement, deed restriction, or comparable legal instrument.

X. Adaptive Management

If results of the monitoring surveys indicate that the mitigation is not successful, the applicant will coordinate with the USACE in an attempt to agree upon the appropriate course of action. In the event of a discreet storm event or other "Act of God", CPA will discuss with the USACE how to best bring the site up to performance standards, or to reach an agreement that the site has achieved significant function and value to replace those at the impact area.

XI. Financial Assurances

Financial Assurances for the mitigation site will be provided via either an escrow account or bond and will be financially-based off the costs associated with Sections VIII and IX, above. The applicant will work with USACE personnel and their environmental consultant to determine an appropriate escrow account amount or bond amount to insure the completion of Sections VIII and IX, above.
EXHIBIT A

Vicinity Map

Plan View

Plan View Notes

Section A-Mitigation Site

Section B-Mitigation Site

Section C-Temporary Access Road Section

Calhoun Port Authority

PERMITTED PLANS

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NOTES:

-See Exhibit A Plan View Notes, pages ____ of __

-Levees will be built with hauled in fill and/or material excavated from within the site adjacent to the levees.

-During construction, the levees may be temporarily built up to an elevation of +10 ft NAVD 88 to accommodate equipment movements. Prior to mitigation site construction completion, the levees will be contoured to final grades as per Sections A & B.

-Within the 3.0-acre levee footprint, the 1.8-acre bayward portion of the levee would be armored with approx.1,775 linear ft of articulated mat to provide stabilization of the levee from wind and wave energy. The finished grade of the armored levee would be +5.0 ft NAVD 88. The finished grade of the 1.2 acres of unarmored levee will be between +2.0 ft and +3.0 ft NAVD 88 to allow for tidal influence. Circulation channels will be lowered to -2.0 to -3.0 ft NAVD 88 with a 20-ft top width. Along with the 1.3-acre high marsh fill within the site, the unarmored levee area would be planted on 3-ft centers with appropriate estuarine species (e.g. smooth cordgrass (Spartina alterniflora) on side slopes and saltgrass (Distichlis spicata), seashore paspalum (Paspalum vaginatum), turtle weed (Batis maritima), chicken claws (Sarcocornia ambigua), sea ox-eye daisy (Borrichia frutescens), etc.) on higher elevations. The 8.7 acres of low marsh creation involves planting smooth cordgrass on 3-ft centers at elevations ranging from +0.5 ft to +1.6 ft NAVD 88. Smooth cordgrass was observed growing in the vicinity from +0.5 ft NAVD 88 to +1.6 ft NAVD 88. Additional surveys will be performed prior to construction. The results will be used to make adjustments to finished grades as warranted.

CALHOUN PORT AUTHORITY PROPOSED MARINE TERMINAL SOUTH PENINSULA DEVELOPMENT PROJECT CALHOUN COUNTY, TEXAS

BELAIRE ENVIRONMENTAL, INC.P.O. Box 741Rockport, Texas 78382June 23, 2020Page ____ of ____

EXHIBIT A- PLAN VIEW NOTES Bean Tract Mitigation Site Calhoun Port Authority Lavaca Bay, Calhoun County, Texas SWG-2016-01066 June 23, 2020

- 1. The maximum footprint of the mitigation site, including levees, will not exceed 14 acres.
- 2. Levees will be built with hauled in fill and/or material excavated from within the site adjacent to the levees.
- 3. During construction, the levees may be temporarily built up to an elevation of +10 ft NAVD 88 to accommodate equipment movements. Prior to mitigation site construction completion, the levees will be contoured to final grades as per Sections A & B.
- 4. Within the 3.0-acre levee footprint, the 1.8-acre bayward portion of the levee would be armored with approximately 1,775 linear ft of articulated mat to provide stabilization of the levee from wind and wave energy. The finished grade of the armored levee would be +5.0 ft NAVD 88. Belaire Environmental, Inc.'s (BEI) past experience indicates that the articulated matting to be used for the proposed 1,775-ft armored breakwater will likely facilitate oyster, barnacle, and other aquatic species attachment. Between 1990 & 2010, BEI planned, permitted, and assisted with installation of four similar BU projects at the Aransas National Wildlife Refuge. Monitoring studies found that all four established substantial oyster populations within the intertidal zone.

The remaining 1.2 acres of unarmored levee will be lowered to between +2.0 ft and +3.0 ft NAVD 88 after consolidation of fill within the site. Circulation channels will be lowered to -2.0 to -3.0 ft NAVD 88 with a 20-ft top width. Along with the 1.3-acre high marsh fill within the site, the levee area would then be planted on 3-ft centers with appropriate estuarine species (e.g. smooth cordgrass (*Spartina alterniflora*) on side slopes and saltgrass (*Distichlis spicata*), seashore paspalum (*Paspalum vaginatum*), turtle weed (*Batis maritima*), chicken claws (*Sarcocornia ambigua*), sea ox-eye daisy (*Borrichia frutescens*), etc.) on higher elevations.

- 5. Depending upon final design, approx. 60,000 to 80,000 cu yds of suitable material from the CPA harbor dredging project will be mechanically or hydraulically dredged then placed within the 14-acre site into a confined leveed area at elevations suitable to create a network of intermixed low and high tidal marshes with circulation channels.
- 6. Within the interior of the finished grade levees, 8.7 ac of low marsh and 1.3 ac high marsh will be contoured and planted with appropriate species. The 8.7 acres of low marsh creation involves planting smooth cordgrass on 3-ft centers at elevations ranging from +0.5 ft to +1.6 ft NAVD 88. Smooth cordgrass was observed growing in the vicinity from +0.5 ft NAVD 88 to +1.6 ft NAVD 88. Additional surveys will be performed prior to construction. The results will be used to make adjustments to finished grades as warranted. Additionally, CPA will also plant high marsh species within targeted grades along the finished grade 1.2-acre unarmored levee in order to aid in stabilization of the levee. In addition to providing stabilization, the planted high marsh areas within the levee footprint will provide increased habitat function and value.

- 7. Mechanically placed material will either be trucked or barged to the site. If land-based mechanical placement of material is used, up to two temporary access roads with 70-ft surface width may be constructed to provide equipment access, including ingress & egress for trucks. Wetlands will be avoided for these temporary access roads. These roads will be removed upon completion of construction and pre-construction contours restored.
- 8. If hydraulic dredging is utilized, interior levees and weirs will be constructed to accommodate settling of TSS. An access route for the dredge pipe that is free of oysters, navigation hazards, and sensitive resources will be staked prior to placement of the dredge pipe.
- 9. BEI conducted an extensive field survey in the area and found no seagrass, oysters, or other sensitive resources within the proposed mitigation site.
- 10. The mitigation site boundary, including levee dimensions, is subject to changes based on further engineering and contractor evaluations. The location of planting benches and circulation channels may be altered due to further evaluation of site conditions.
- 11. The mitigation site area is owned by the Calhoun Port Authority.
- 12. As verified by the USACE in JD SWG-2016-01066 on Sept. 25, 2017.MHW= +1.30 ft NAVD88 AHTL=+2.90 ft NAVD88. MLLW= 0.48 ft NAVD 88.









NOTES:

-Up to two temporary roads with 70 foot surface width are proposed to be constructed to provide equipment access if land based mechanical placement of material is used. Precise location and dimensions may vary depending upon site conditions.

-Wetlands will be avoided for these proposed access roads.

-All elevations shown in feet, NAVD 88. Mean High Water (MHW)= +1.30 ft NAVD88 Annual High Tide (AHT) Line= +2.90 ft NAVD88. These elevations were verified by the USACE within JD SWG-2016-01066 on Sept. 25, 2017. MLLW=+0.48 ft NAVD 88

-For permitting only, not for construction.

-Prepared by Belaire Environmental, Inc. on January 16, 2020 (JAM). Rev. June 23, 2020

Jon Niermann, *Chairman* Emily Lindley, *Commissioner* Bobby Janecka, *Commissioner* Toby Baker, *Executive Director*



TEXAS COMMISSION ON ENVIRONMENTAL QUALITY

Protecting Texas by Reducing and Preventing Pollution

September 4, 2020

Ms. Kara Vick Galveston District CESWG-PE-RE U.S. Army Corps of Engineers P.O. Box 1229 Galveston, Texas 77553-1229

Re: USACE Permit Application No. SWG-2016-01066

Dear Ms. Vick:

This letter is in response to the Statement of Findings (SOF) dated August 27, 2020, for the Joint Public Notice dated December 27, 2018, on the Calhoun Port Authority's (CPA) proposed marine terminal for liquid petrochemicals, and the construction of a 61-acre dredge material stockpile area to create an adjacent uplands area for future port expansion. The project is in Lavaca Bay and adjacent wetlands adjacent to the Port of Port Lavaca-Point Comfort, Point Comfort, Calhoun County, Texas.

The Texas Commission on Environmental Quality (TCEQ) has reviewed the public notice and related application information along with the SOF. On behalf of the Executive Director and based on our evaluation of the information contained in these documents, the TCEQ certifies that there is reasonable assurance that the project will be conducted in a way that will not violate water quality standards. General information regarding this water quality certification, including standard provisions of the certification, is included as an attachment to this letter.

For the marine terminal, the applicant proposes to mechanically dredge 2.615 million cubic yards (MCY) of material to a depth of 47 feet that will impact approximately 40.75 acres of open waters and 0.83 acres of marine emergent wetlands. For the uplands expansion, the applicant will fill approximately 11.95 acres of adjacent estuarine emergent wetlands and 21 acres of open waters.

To offset wetland impacts, the applicant proposes permittee-responsible mitigation at the applicant-owned property referred to as the Bean Tract in Lavaca Bay. The final mitigation plan dated August 4, 2020, states that low and high marsh areas will be established, and an approximately 1,775-foot hard substrate breakwater will be constructed.

The TCEQ has reviewed this proposed action for consistency with the Texas Coastal Management Program (CMP) goals and policies in accordance with the CMP regulations

P.O. Box 13087 • Austin, Texas 78711-3087 • 512-239-1000 • tceq.texas.gov

Ms. Kara Vick U.S. Army Corps of Engineers USACE Permit Application No. SWG-2016-01066 Page 2

(Title 31, Texas Administrative Code (TAC), Section (§)505.30) and has determined that the action is consistent with the applicable CMP goals and policies.

This certification was reviewed for consistency with the CMP's development in critical areas policy (31 TAC §501.23) and dredging and dredged material disposal and placement policy (31 TAC §501.25). This certification complies with the CMP goals (31 TAC §501.12(1, 2, 3, 5)) applicable to these policies.

No review of property rights, location of property lines, nor the distinction between public and private ownership has been made, and this certification may not be used in any way with regard to questions of ownership.

If you require additional information or further assistance, please contact Dr. Mary Anne Wallace, Water Quality Assessment Section, Water Quality Division (MC-150), at (512) 239-4604 or by email at *Mimi.Wallace@tceq.texas.gov*.

Sincerely,

David W Caludo

David W. Galindo Water Quality Division Director Texas Commission on Environmental Quality

DWG/MAW/__

Attachment

ccs: Charles R. Hausmann, Calhoun Port Authority, via e-mail at crh@calhounport.com Ms. Allison Buchtien, via e-mail at Federal.Consistency@GLO.TEXAS.GOV **WORK DESCRIPTION:** As described in the public notice dated December 27, 2018, and the August 27, 2020, Environmental Assessment and Statement of Findings.

SPECIAL CONDITIONS: None

GENERAL: This certification, issued pursuant to the requirements of Title 30, Texas Administrative Code, Chapter 279, is restricted to the work described in the August 27, 2020, Environmental Assessment and Statement of Findings and shall be concurrent with the Corps of Engineers (COE) permit. This certification may be extended to any minor revision of the COE permit when such change(s) would not result in an impact on water quality. <u>The Texas Commission on Environmental Quality (TCEQ) reserves the right</u> to require full joint public notice on a request for minor revision. The applicant is hereby placed on notice that any activity conducted pursuant to the COE permit which results in a violation of the state's surface water quality standards may result in an enforcement proceeding being initiated by the TCEQ or a successor agency.

STANDARD PROVISIONS: These following provisions attach to any permit issued by the COE and shall be followed by the permittee or any employee, agent, contractor, or subcontractor of the permittee during any phase of work authorized by a COE permit.

- 1. The water quality of wetlands shall be maintained in accordance with all applicable provisions of the Texas Surface Water Quality Standards including the General, Narrative, and Numerical Criteria.
- 2. The applicant shall not engage in any activity which will cause surface waters to be toxic to man, aquatic life, or terrestrial life.
- 3. Permittee shall employ measures to control spills of fuels, lubricants, or any other materials to prevent them from entering a watercourse. All spills shall be promptly reported to the TCEQ by calling the State of Texas Environmental Hotline at 1-800-832-8224.
- 4. Sanitary wastes shall be retained for disposal in some legal manner. Marinas and similar operations which harbor boats equipped with marine sanitation devices shall provide state/federal permitted treatment facilities or pump out facilities for ultimate transfer to a permitted treatment facility. Additionally, marinas shall display signs in appropriate locations advising boat owners that the discharge of sewage from a marine sanitation device to waters in the state is a violation of state and federal law.
- 5. Materials resulting from the destruction of existing structures shall be removed from the water or areas adjacent to the water and disposed of in some legal manner.
- 6. A discharge shall not cause substantial and persistent changes from ambient conditions of turbidity or color. The use of silt screens or other appropriate methods is encouraged to confine suspended particulates.

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- 7. The placement of any material in a watercourse or wetlands shall be avoided and placed there only with the approval of the Corps when no other reasonable alternative is available. If work within a wetland is unavoidable, gouging or rutting of the substrate is prohibited. Heavy equipment shall be placed on mats to protect the substrate from gouging and rutting if necessary.
- 8. Dredged Material Placement: Dredged sediments shall be placed in such a manner as to prevent any sediment runoff onto any adjacent property not owned by the applicant. Liquid runoff from the disposal area shall be retained on-site or shall be filtered and returned to the watercourse from which the dredged materials were removed. Except for material placement authorized by this permit, sediments from the project shall be placed in such a manner as to prevent any sediment runoff into waters in the state, including wetlands.
- 9. If contaminated spoil that was not anticipated or provided for in the permit application is encountered during dredging, dredging operations shall be immediately terminated and the TCEQ shall be contacted by calling the State of Texas Environmental Hotline at 1-800-832-8224. Dredging activities shall not be resumed until authorized by the Commission.
- 10. Contaminated water, soil, or any other material shall not be allowed to enter a watercourse. Noncontaminated storm water from impervious surfaces shall be controlled to prevent the washing of debris into the waterway.
- 11. Storm water runoff from construction activities that result in a disturbance of one or more acres, or are a part of a common plan of development that will result in the disturbance of one or more acres, must be controlled and authorized under Texas Pollutant Discharge Elimination System (TPDES) general permit TXR150000. A copy of the general permit, application (notice of intent), and additional information is available at:

http://www.tceq.texas.gov/permitting/stormwater/construction or by contacting the TCEQ Stormwater Team at (512) 239-4671.

- 12. Upon completion of earthwork operations, all temporary fills shall be removed from the watercourse/wetland, and areas disturbed during construction shall be seeded, riprapped, or given some other type of protection to minimize subsequent soil erosion. Any fill material shall be clean and of such composition that it will not adversely affect the biological, chemical, or physical properties of the receiving waters.
- 13. Disturbance to vegetation will be limited to only what is absolutely necessary. After construction, all disturbed areas will be revegetated to approximate the predisturbance native plant assemblage.

- 14. Where the control of weeds, insects, and other undesirable species is deemed necessary by the permittee, control methods which are nontoxic to aquatic life or human health shall be employed when the activity is located in or in close proximity to water, including wetlands.
- 15. Concentrations of taste and odor producing substances shall not interfere with the production of potable water by reasonable water treatment methods, impart unpalatable flavor to food fish including shellfish, result in offensive odors arising from the water, or otherwise interfere with reasonable use of the water in the state.
- 16. Surface water shall be essentially free of floating debris and suspended solids that are conducive to producing adverse responses in aquatic organisms, putrescible sludge deposits, or sediment layers which adversely affect benthic biota or any lawful uses.
- 17. Surface waters shall be essentially free of settleable solids conducive to changes in flow characteristics of stream channels or the untimely filling of reservoirs, lakes, and bays.
- 18. The work of the applicant shall be conducted such that surface waters are maintained in an aesthetically attractive condition and foaming or frothing of a persistent nature is avoided. Surface waters shall be maintained so that oil, grease, or related residue will not produce a visible film of oil or globules of grease on the surface or coat the banks or bottoms of the watercourse.
- 19. This certification shall not be deemed as fulfilling the applicant's/permittee's responsibility to obtain additional authorization/approval from other local, state, or federal regulatory agencies having special/specific authority to preserve and/or protect resources within the area where the work will occur.